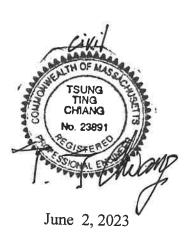
# DRAINAGE SUMMARY 2202 COMMONWEALTH AVENUE NEWTON, MASSACHUSETTS



Lakeview Engineering Associates P.O. Box 787 Hudson, Massachusetts 01749

# DRAINAGE SUMMARY 2202 COMMONWEALTH AVENUE NEWTON, MASSACHUSETTS

The proposed project consists of the re-development of an existing, single family house lot at 2202 Commonwealth Avenue into a multi-family project, under the requirements of the City of Newton, including Stormwater Management & Erosion Control requirements. The proposed project includes the demolition of the existing structure & driveway and the construction of a new five unit condominium building, site grading, retaining walls, driveway and associated work. Overall, the proposed impervious area on the lot will be approximately 65.4% greater than existing conditions, due to the new building footprint, access driveway & parking area. The on-line soil survey for the area shows "Merrimack Urban Land Complex" soils which are a Class A sand / gravel as the predominant soils for the area. The on-site soil evaluation determined the soils to be similar to the Merrimack description, with sandy loam above & below the primary soil. Under State Stormwater Management guidelines would be considered a Class A soil. Typically these soils would have a "Rawls" rate of 0.0115 feet / minute. As such, the drainage controls have been designed with the standard "Rawls" infiltration rate component for the Merrimack soils, for both pre & post runoff calculations.

Existing ground cover on the site is a typical residential lawn area, in relatively average conditions around the house, with few trees. The drainage on the site from the rear area is to Commonwealth Avenue. The proposed grading and flow paths will be similar to the existing conditions, with more impervious surface due to the larger building footprint. Overall, the site will maintain the current flow patterns, with the building roof and the majority of the driveway, as well as a portion of the rear lawn being collected and discharged to the infiltration system. There are no wetland resource areas on or near the site. The proposed project will maintain the existing, residential use in the area. The proposed drainage controls are designed to capture & contain the roof area, the driveway & a portion of the rear lawn area. The roof runoff will be collected by the roof leader collection piping, which will discharge to the infiltration system. This system will store a large portion of the runoff from these areas and allow the stored water to slowly infiltrate during & after the storm event.

As noted, the design soil at the site is a coarse, sandy material. Under the proposed conditions, with the site being developed and loamed & seeded and the use of the infiltration system, the rate & volume of site runoff from the existing lot will be reduced for all design storm events. The reduction in rate & volume over the existing conditions, meets the City's requirement to handle the differential increase in runoff, as well as store a minimum of two inches of runoff from the total impervious area of the new project. In addition, the proposed controls will provide some additional, long term recharge of the groundwater at the site.

Tables No. 1 & 2 provides a summary of the existing and proposed conditions used in the runoff calculations.

# Table No. 1 - Existing Conditions

Subcatchment	Ground <u>Cover</u>	Curve <u>Number</u>	Area (Sq. Ft.)	Tc (Min.)	Comments
A-1	Ex. Site	64	13,696	6.6	Incl. Roof, Drive, Walks & Walls & Lawn Area

Total Imp. Area= 4,127 Sq. Ft.

# Table No. 2 - Proposed Conditions

Subcatchmen	nt Ground <u>Cover</u>	Curve <u>Number</u>	Area (Sq. Ft.)	Tc ( <u>Min.)</u>	Comments
B-1	Prop. Imp. Lawn	98 39	1,952 4,887	5.0	Drive & Walk
B-2	Prop. Imp.	98	4,876	5.0	Roof, Walks,
	Lawn	74	1,242	5.0	Drives & Walls

Total Imp. Area= 6,828 Sq. Ft.

The runoff conditions at the site were evaluated for both pre and post-development conditions using the SCS TR-20 based Hydrocad computer program. Based on this evaluation (see attached) and as noted above, it is evident that the proposed work will be able to maintain a similar runoff flow pattern as exists today, with reduced rate & volume for up to the 100 year storm event, with the exception of a minor rate increase for the 100 year storm. The following summarizes the results of the computer evaluation under pre, post and controlled conditions:

# **EXISTING CONDITIONS**

### Storm Event Runoff (Rate/Volume)

Drainage Area	2 Yr. Storm (cfs/af)	10 Yr. Storm (cfs/af)	25 Yr. Storm (cfs/af)	100 Yr. Storm (cfs/af)
Subcatchment A-1	0.16 / 0.014	0.57 / 0.040	0.88 / 0.061	1.57 / 0.107

# POSTDEVELOPMENT RUNOFF CONDITIONS

### Storm Event Runoff (Rate/Volume)

Drainage Area	2 Yr. Storm	10 Yr. Storm	25 Yr. Storm	100 Yr. Storm
	(cfs/af)	(cfs/af)	(cfs/af)	(cfs/af)
Subcatchment B-1	0.02 / 0.003	0.18 / 0.013	0.31 / 0.021	0.62 / 0.042
Subcatchment B-2	0.28 / 0.019	0.58 / 0.039	0.77 / 0.052	1.17 / 0.080
Non-Weighted Summary	0.30 / 0.022	0.76 / 0.042	1.08 / 0.073	1.79 / 0.122

# CONTROLLED POSTDEVELOPMENT CONDITIONS\*

### Storm Event Runoff (Rate/Volume)

Drainage Area	2 Yr. Storm (cfs/af)	10 Yr. Storm (cfs/af)	25 Yr. Storm (cfs/af)	100 Yr. Storm (cfs/af)
Subcatchment B-1 Pond # 1 (B-2)	0.02 / 0.003 0.00 / 0.000	0.18 / 0.013 <u>0.00 / 0.000</u>	0.31 / 0.021 0.00 / 0.000	0.62 / 0.042 1.51 / 0.013
Totals (Weighted)**	0.02 / 0.003	0.18 / 0.013	0.31 / 0.021	1.99 / 0.055

<sup>\*</sup> As modified by the Infiltration Systems for Subcatchment B-2!

# PRE & POST-DEVELOPMENT RUNOFF SUMMARY

### Storm Event Runoff (Rate/Volume)

Drainage Area	2 Yr. Storm (cfs/af)	10 Yr. Storm (cfs/af)	25 Yr. Storm (cfs/af)	100 Yr. Storm (cfs/af)
Predevelopment	0.16 / 0.014	0.57 / 0.040	0.88 / 0.061	1.57 / 0.107
Postdevelopment	0.02 / 0.003	0.18 / 0.013	0.31 / 0.021	1.99 / 0.055

<sup>\*\*</sup> Totals are Time Weighted per Summary Node

As noted above, the subsurface stormwater infiltration system will contain a large portion of site runoff & infiltrate most of the site runoff during the storm event and after the storm ceases, maintaining discharge rates and volumes below existing conditions, with the exception of a minor rate increase for the 100 year storm. Currently, the site discharges to the street. The new site will maintain this flow pattern with a greatly reduced volume of runoff. The infiltration system will infiltrate runoff volume during and after the storm event due to the retained volume of runoff below the outlet, for additional groundwater recharge. This infiltrated volume more than approximates the infiltration volume of the existing site conditions that will be replaced with the new developed surfaces.

# **City Infiltration Requirement:**

The City of Newton has adopted an additional requirement for projects with regard to retention & infiltration of runoff, based on the project type. The proposed project falls within the criteria of a "Minor Stormwater Permit" with a teardown and construction of a new dwelling & site work, as such, the City requires that the equivalent of two (2) inches of runoff from the total impervious area of the site be retained & infiltrated. The proposed on-site infiltration system will meet this requirement, as follows:

# Total Proposed Impervious Area (See Table 2)- 6,828 Square Feet!

Retention Requirement: Two (2) inch rainfall event. As per the 2" rainfall event attached, the total runoff from the site is 0 cubic feet, which meets this requirement!

# State Stormwater Standards:

The Massachusetts DEP has developed a set of standards that have been adopted by the City as part of their Stormwater Management and Erosion Control Rules & Regulations. These standards and the projects compliance are noted as follows:

# Standard No. 1 - Untreated Stormwater

The project does not propose any new stormwater runoff discharge from the site that is not treated prior to discharge.

# Standard No. 2 - Postdevelopment Peak Runoff Increase

The project does not proposed any increase in stormwater runoff rates or volumes, as noted above in the Pre & Post Development Runoff Summary, with the exception of a small increase of peak rate during the 100 year storm.

# Standard No. 3 - Recharge to Groundwater

The proposed impervious area of 6,828 sq. ft. or 0.157 acres times 0.60 inches or 0.0079 acre feet required recharge for a Class A soil = 0.0079 acre feet (344 cu. ft.). The storage within the infiltration system is 655 cu. ft. which meets this requirement.

# Standard No. 4 - Water Quality

The project requires a minimum of 0.5 inch of runoff times the impervious area of the site to be treated for solids removal and that an average of 80% removal be accomplished for the project. The majority of the proposed impervious area for the project is treated by the infiltration system which has a treatment level of 80%.

# Standard No. 5 - Land Use with Potentially Higher Pollutant Loading

The project is a residential use lot and does not have any potential for higher pollutant load levels.

# Standard No. 6 - Water Quality Treatment

The project is a residential use lot and does not discharge to any critical resource area.

# Standard No. 7 - Redevelopment Projects

The project is a demolition & redevelopment of the residential use and meets the standard as well as the City requirements.

# Standard No. 8 - Erosion Control

The project has erosion controls incorporated into the work.

# Standard No. 9 - Operation & Maintenance Plan

The project is has a proposed O & M plan for all aspects of the design.

# Standard No. 10 - Potential Illicit Discharges

The project is a residential use lot and does not have potential for illicit discharges.











### 2202 Comm. Ave. Pre

Type III 24-hr Rainfall=3.29" (2 Yr. Storm)

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Page 2

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Type III 24-hr Rainfall=3.29"

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment A-1: Existing Lot to Street** 

Tc=6.6 min CN=64 Area=13,696 sf Runoff= 0.16 cfs 0.014 af

Runoff Area = 0.314 ac Volume = 0.014 af Average Depth = 0.53"

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# **Subcatchment A-1: Existing Lot to Street**

Runoff

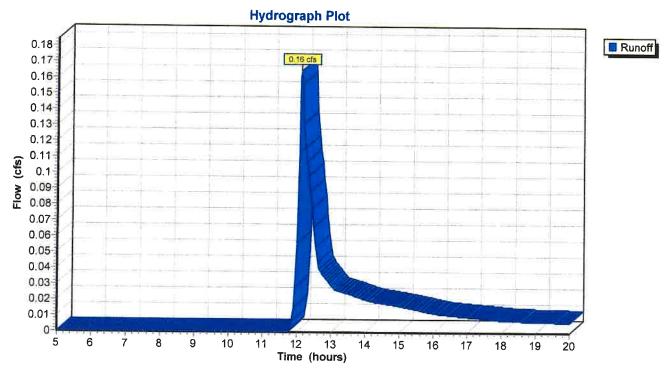
0.16 cfs @ 12.12 hrs, Volume=

0.014 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=3.29"

A	rea (sf)	CN E	escription					
	4,127	98 Paved parking & roofs						
	9,569				Fair, HSG A			
	13,696		Veighted A					
			9	35				
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
3.8	39	0.0330	0.2		Sheet Flow, Overland Flow			
					Grass: Short n= 0.150 P2= 3.20"			
1.9	20	0.0500	0.2		Sheet Flow, Overland Flow			
					Grass: Short n= 0.150 P2= 3.20"			
0.6	41	0.0240	1.1		Shallow Concentrated Flow, Overland Flow			
					Short Grass Pasture Kv= 7.0 fps			
0.3	28	0.0710	1.9		Shallow Concentrated Flow, Overland Flow			
					Short Grass Pasture Kv= 7.0 fps			
0.0	11	0.4500	4.7		Shallow Concentrated Flow, Overland Flow			
					Short Grass Pasture Kv= 7.0 fps			
6.6	139	Total						

### **Subcatchment A-1: Existing Lot to Street**



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Page 4 5/30/2023

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Type III 24-hr Rainfall=5.17"
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment A-1: Existing Lot to Street

Tc=6.6 min CN=64 Area=13,696 sf Runoff= 0.57 cfs 0.040 af

Runoff Area = 0.314 ac Volume = 0.040 af Average Depth = 1.54"

Page 5 5/30/2023

# **Subcatchment A-1: Existing Lot to Street**

Runoff

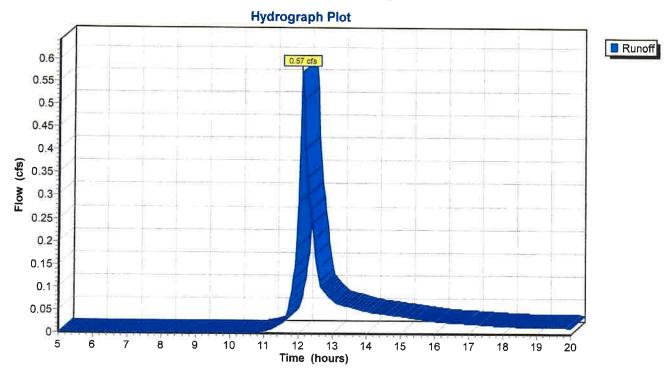
0.57 cfs @ 12.11 hrs, Volume=

0.040 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=5.17"

	A	rea (sf)	CN [	Description								
		4,127	98 F	98 Paved parking & roofs								
		9,569										
		13,696		Veighted A								
				•								
	Tc	Length	Slope	Velocity	Capacity	Description						
	(min)_	(feet)	(ft/ft)	(ft/sec)	(cfs)	•						
	3.8	39	0.0330	0.2		Sheet Flow, Overland Flow						
						Grass: Short n= 0.150 P2= 3.20"						
	1.9	20	0.0500	0.2		Sheet Flow, Overland Flow						
						Grass: Short n= 0.150 P2= 3.20"						
	0.6	41	0.0240	1.1		Shallow Concentrated Flow, Overland Flow						
	0.0					Short Grass Pasture Kv= 7.0 fps						
	0.3	28	0.0710	1.9		Shallow Concentrated Flow, Overland Flow						
	0.0	4.4	0.4500			Short Grass Pasture Kv= 7.0 fps						
	0.0	11	0.4500	4.7		Shallow Concentrated Flow, Overland Flow						
9						Short Grass Pasture Kv= 7.0 fps						
	6.6	139	Total									

### Subcatchment A-1: Existing Lot to Street



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Page 6 5/30/2023

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Type III 24-hr Rainfall=6.35"
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment A-1: Existing Lot to Street** 

Tc=6.6 min CN=64 Area=13,696 sf Runoff= 0.88 cfs 0.061 af

Runoff Area = 0.314 ac Volume = 0.061 af Average Depth = 2.31"

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# **Subcatchment A-1: Existing Lot to Street**

Runoff

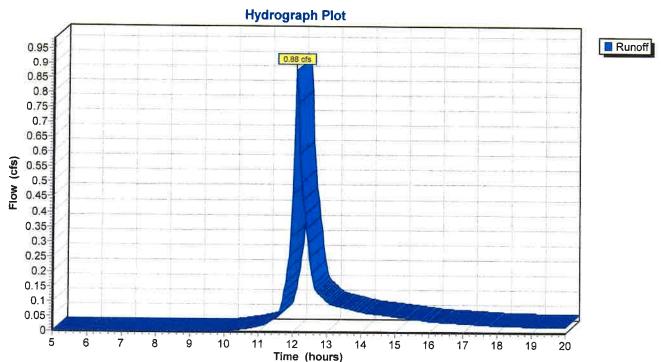
0.88 cfs @ 12.10 hrs, Volume=

0.061 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=6.35"

	Α	rea (sf)	CN [	Description						
		4,127 98 Paved parking & roofs								
		9,569	49 5	50-75% Gra	ass cover, I	Fair, HSG A				
		13,696		Neighted A						
				•	Ü					
	Tc	Length	Slope	Velocity	Capacity	Description				
2	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	•				
	3.8	39	0.0330	0.2		Sheet Flow, Overland Flow				
						Grass: Short n= 0.150 P2= 3.20"				
	1.9	20	0.0500	0.2		Sheet Flow, Overland Flow				
						Grass: Short n= 0.150 P2= 3.20"				
	0.6	41	0.0240	1.1		Shallow Concentrated Flow, Overland Flow				
						Short Grass Pasture Kv= 7.0 fps				
	0.3	28	0.0710	1.9		Shallow Concentrated Flow, Overland Flow				
		4.4				Short Grass Pasture Kv= 7.0 fps				
	0.0	11	0.4500	4.7		Shallow Concentrated Flow, Overland Flow				
						Short Grass Pasture Kv= 7.0 fps				
	6.6	139	Total							

### Subcatchment A-1: Existing Lot to Street



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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Type III 24-hr Rainfall=8.78"
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment A-1: Existing Lot to Street

Tc=6.6 min CN=64 Area=13,696 sf Runoff= 1.57 cfs 0.107 af

Runoff Area = 0.314 ac Volume = 0.107 af Average Depth = 4.10"

# **Subcatchment A-1: Existing Lot to Street**

Runoff

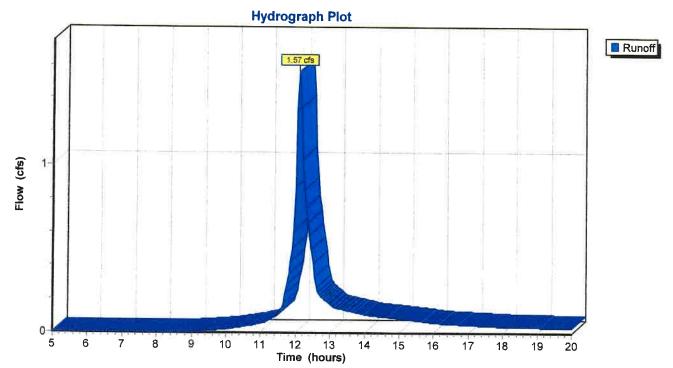
1.57 cfs @ 12.10 hrs, Volume=

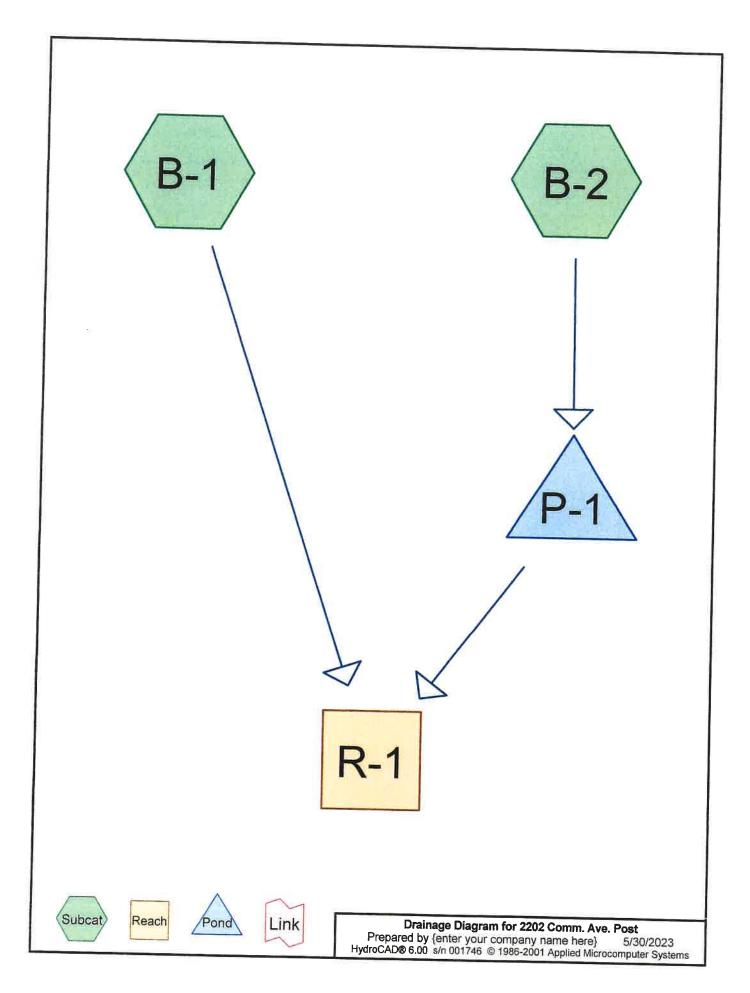
0.107 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=8.78"

A	rea (sf)	CN E	Description							
	4,127	98 F	98 Paved parking & roofs							
	9,569				Fair, HSG A					
	13,696		Veighted A							
	·									
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	=					
3.8	39	0.0330	0.2		Sheet Flow, Overland Flow					
					Grass: Short n= 0.150 P2= 3.20"					
1.9	20	0.0500	0.2		Sheet Flow, Overland Flow					
					Grass: Short n= 0.150 P2= 3.20"					
0.6	41	0.0240	1.1		Shallow Concentrated Flow, Overland Flow					
					Short Grass Pasture Kv= 7.0 fps					
0.3	28	0.0710	1.9		Shallow Concentrated Flow, Overland Flow					
					Short Grass Pasture Kv= 7.0 fps					
0.0	11	0.4500	4.7		Shallow Concentrated Flow, Overland Flow					
					Short Grass Pasture Kv= 7.0 fps					
6.6	139	Total								

# **Subcatchment A-1: Existing Lot to Street**





# **Subcatchment B-1: Tributary to Street**

Runoff

0.00

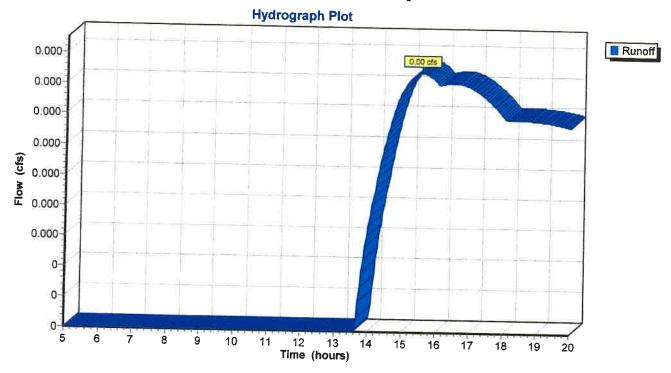
0.00 cfs @ 15.56 hrs, Volume=

0.000 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=2.00"

A	rea (sf)	CN	Description			
	1,952	98	Paved park	ing & roofs		
	4,887	39	>75% Gras	s cover, Go	ood, HSG A	
	6,839	56	Neighted A	verage		
_			_	J		
Tc	Length	Slope	01000	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·	
5.0					Direct Entry, Overland Flow	

# Subcatchment B-1: Tributary to Street



# Subcatchment B-2: Tributary to Infiltration

Runoff

=

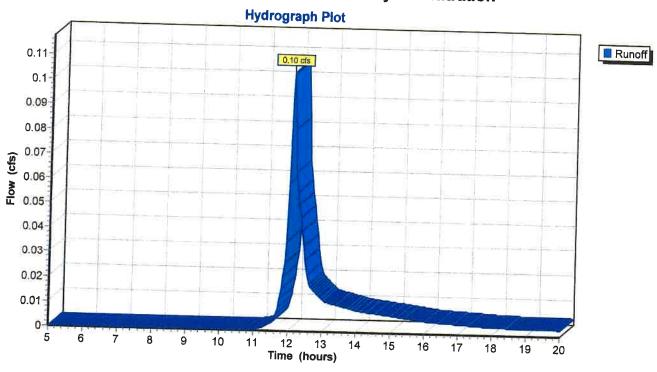
0.10 cfs @ 12.09 hrs, Volume=

0.007 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=2.00"

A	rea (sf)	CN	Description			
3	4,876 1,981	98 39	Paved park >75% Gras	ing & roofs	ood, HSG A	
	6,857	81	Weighted A	verage	500, 115G A	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description	
5.0					Direct Entry, Overland Flow	

# Subcatchment B-2: Tributary to Infiltration



Page 3 5/30/2023

# Reach R-1: Summary Node

Inflow = Outflow =

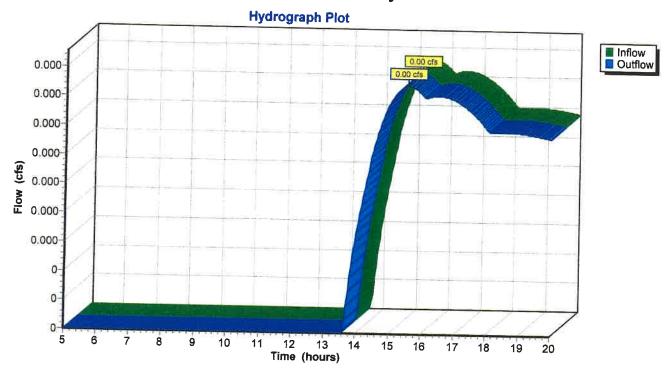
0.00 cfs @ 15.56 hrs, Volume= 0.00 cfs @ 15.56 hrs, Volume=

0.000 af

0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

# Reach R-1: Summary Node



Page 4 5/30/2023

# Pond P-1: Infiltration System

Inflow = Outflow = Discarded = Primary =	0.10 cfs @ 0.10 cfs @	12.09 hrs, Volume= 12.11 hrs, Volume= 12.11 hrs, Volume= 5.00 hrs, Volume=	0.007 af,	Atten= 1%,	Lag= 1.0 min
--	--------------------------	---	-----------	------------	--------------

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 74.32' Storage= 6 cf

Plug-Flow detention time= 1.0 min calculated for 0.007 af (100% of inflow)

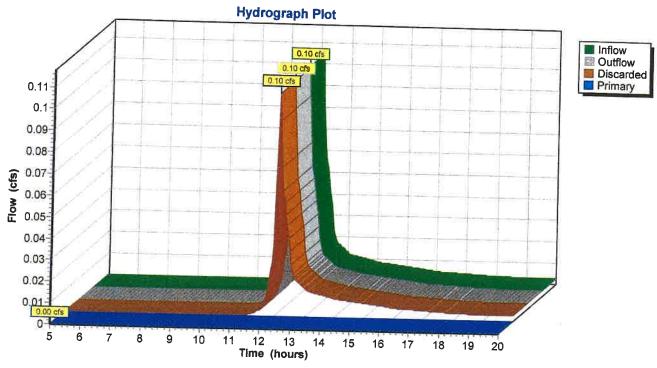
Elevation (feet)	Cum.Store (cubic-feet)
74.30	0
74.80	126
75.97	540
76.47	591
77.60	655

# **Discarded OutFlow** (Free Discharge) 2=Exfiltration

# Primary OutFlow (Free Discharge) 1=Broad-Crested Rectangular Weir

#_	Routing	Invert	Outlet Devices
1	Primary		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 2.00
2	Discarded		Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 0.14 cfs Exfiltration when above invert

Pond P-1: Infiltration System



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Page 2 5/30/2023

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Type III 24-hr Rainfall=3.29"
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment B-1: Tributary to Street

Tc=5.0 min CN=56 Area=6,839 sf Runoff= 0.02 cfs 0.003 af

Subcatchment B-2: Tributary to Infiltration

Tc=5.0 min CN=81 Area=6,857 sf Runoff= 0.28 cfs 0.019 af

Reach R-1: Summary Node

Inflow= 0.02 cfs 0.003 af Outflow= 0.02 cfs 0.003 af

Pond P-1: Infiltration System Peak

Peak Storage= 79 cf Inflow= 0.28 cfs 0.019 af

Discarded= 0.14 cfs 0.019 af Primary= 0.00 cfs 0.000 af Outflow= 0.14 cfs 0.019 af

Runoff Area = 0.314 ac Volume = 0.022 af Average Depth = 0.85"

5/30/2023

# **Subcatchment B-1: Tributary to Street**

Runoff

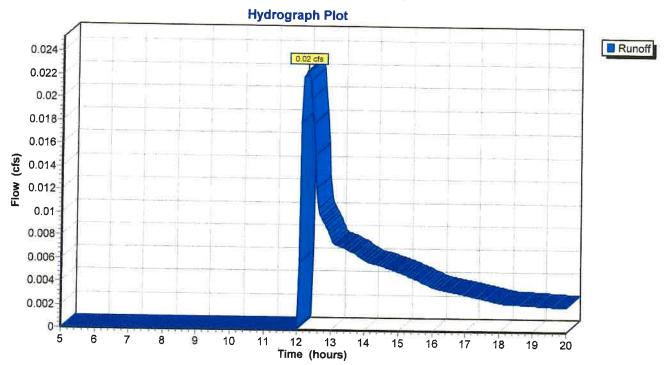
0.02 cfs @ 12.27 hrs, Volume=

0.003 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=3.29"

A	rea (sf)	CN	Description				
	1,952	98	Paved parking & roofs				
	4,887	39	>75% Grass cover, Good, HSG A				
	6,839		Weighted A				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity	Capacity (cfs)	Description		
5.0					Direct Entry, Overland Flow		

# **Subcatchment B-1: Tributary to Street**



5/30/2023

# **Subcatchment B-2: Tributary to Infiltration**

Runoff

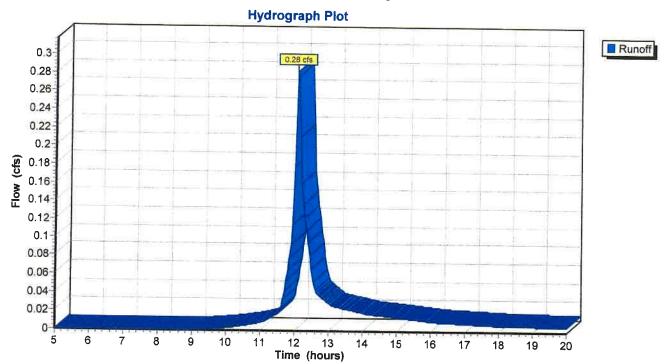
0.28 cfs @ 12.08 hrs, Volume=

0.019 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=3.29"

A	rea (sf)	CN	Description				
	4,876		Paved parking & roofs				
-	1,981	39	>75% Grass cover, Good, HSG A				
	6,857		Weighted A				
Tc (min)	Length (feet)	Slope (ft/ft	,	Capacity (cfs)	Description		
5.0					Direct Entry, Overland Flow		

### **Subcatchment B-2: Tributary to Infiltration**



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Page 5

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### Reach R-1: Summary Node

Inflow =

0.02 cfs @ 12.27 hrs, Volume=

0.003 af

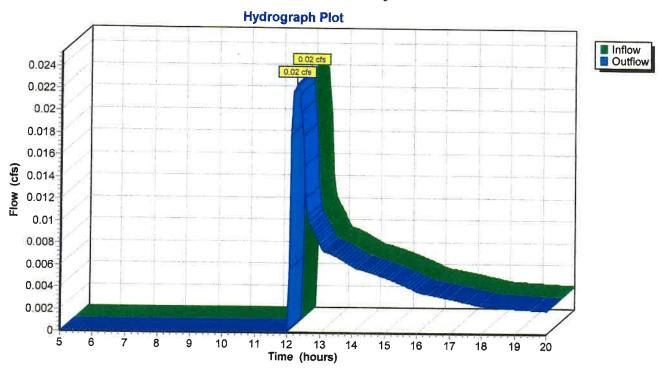
Outflow =

0.02 cfs @ 12.27 hrs, Volume=

0.003 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

### Reach R-1: Summary Node



Type III 24-hr Rainfall=3.29" (2 Yr. Storm)

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Page 6

5/30/2023

# Pond P-1: Infiltration System

Inflow	=	0.28 cfs @	12.08 hrs.	Volume=	0.019 af	
Outflow	=	0.14 cfs @	12.00 hrs.			Atten= 51%, Lag= 0.0 min
Discarded		0.14 cfs @			0.019 af	7 ttteii - 3170, Lag- 0.0 iiiii
Primary		0.00 cfs @			0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 74.61' Storage= 79 cf

Plug-Flow detention time= 3.1 min calculated for 0.019 af (100% of inflow)

Elevation	Cum.Store
(feet)	(cubic-feet)
74.30	0
74.80	126
75.97	540
76.47	591
77.60	655

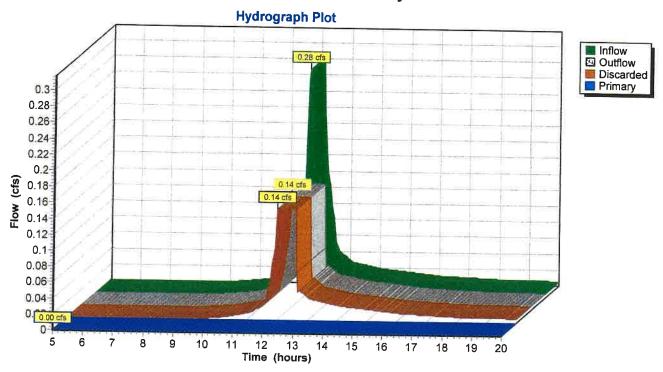
# **Discarded OutFlow** (Free Discharge) 2=Exfiltration

# Primary OutFlow (Free Discharge) 1=Broad-Crested Rectangular Weir

#	Routing	Invert	Outlet Devices
1	Primary	77.50'	12.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32
2	Discarded	74.30'	0.14 cfs Exfiltration when above invert

5/30/2023

Pond P-1: Infiltration System



Page 7

5/30/2023

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Type III 24-hr Rainfall=5.17"
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment B-1: Tributary to Street

Tc=5.0 min CN=56 Area=6,839 sf Runoff= 0.18 cfs 0.013 af

Subcatchment B-2: Tributary to Infiltration

Tc=5.0 min CN=81 Area=6,857 sf Runoff= 0.58 cfs 0.039 af

Reach R-1: Summary Node

Inflow= 0.18 cfs 0.013 af

Outflow= 0.18 cfs 0.013 af

Pond P-1: Infiltration System

Peak Storage= 389 cf Inflow= 0.58 cfs 0.039 af

Discarded= 0.14 cfs 0.039 af Primary= 0.00 cfs 0.000 af Outflow= 0.14 cfs 0.039 af

Runoff Area = 0.314 ac Volume = 0.052 af Average Depth = 1.98"

# **Subcatchment B-1: Tributary to Street**

Runoff

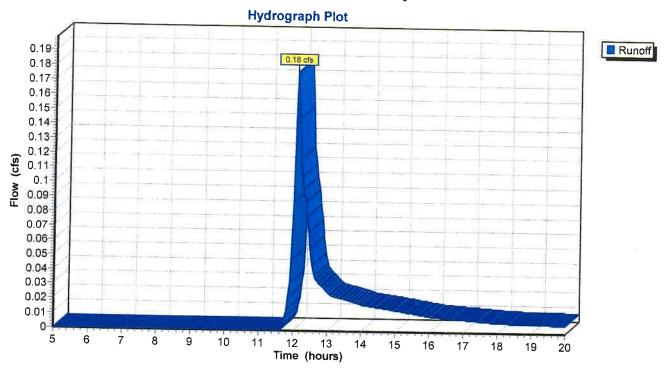
0.18 cfs @ 12.10 hrs, Volume=

0.013 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=5.17"

A	rea (sf)	CN	Description				
	1,952	98	Paved park	Paved parking & roofs			
	4,887	39		>75% Grass cover, Good, HSG A			
	6,839		Weighted A				
Tc (min)	Length (feet)	Slop (ft/f		Capacity (cfs)	Description		
5.0					Direct Entry, Overland Flow		

# Subcatchment B-1: Tributary to Street



Page 9

5/30/2023

# **Subcatchment B-2: Tributary to Infiltration**

Runoff

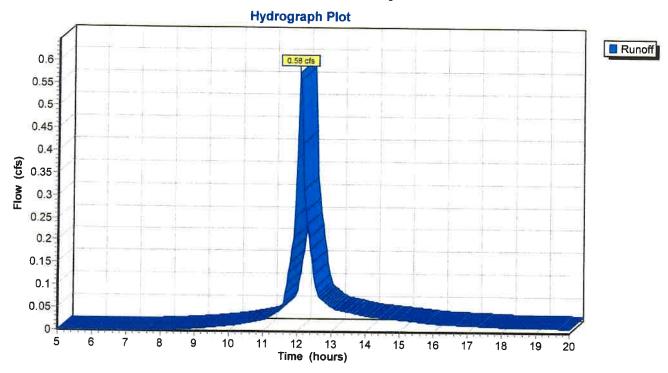
0.58 cfs @ 12.08 hrs, Volume=

0.039 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=5.17"

A	rea (sf)	CN	Description				
	4,876	98	Paved parking & roofs				
	1,981		>75% Grass cover, Good, HSG A				
	6,857		Weighted A				
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description		
5.0					Direct Entry, Overland Flow		

# **Subcatchment B-2: Tributary to Infiltration**



Page 10

5/30/2023

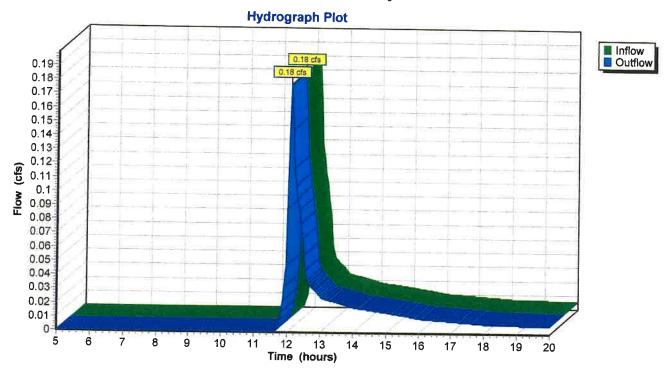
# Reach R-1: Summary Node

Inflow 0.18 cfs @ 12.10 hrs, Volume= 0.013 af

Outflow 0.18 cfs @ 12.10 hrs, Volume= 0.013 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

### Reach R-1: Summary Node



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Page 11

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5/30/2023

# Pond P-1: Infiltration System

Inflow	=	0.58 cfs @	12.08 hrs,	Volume=	0.039 af		
Outflow		0.14 cfs @				Atten= 76%, Lag= 0.0 n	nin
Discarded		0.14 cfs @			0.039 af	7 Mar. 1070, 2ag 0.01	
Primary	=	0.00 cfs @	5.00 hrs,	Volume=	0.000 af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 75.54' Storage= 389 cf

Plug-Flow detention time= 15.9 min calculated for 0.038 af (100% of inflow)

Elevation	Cum.Store
(feet)	(cubic-feet)
74.30	0
74.80	126
75.97	540
76.47	591
77.60	655

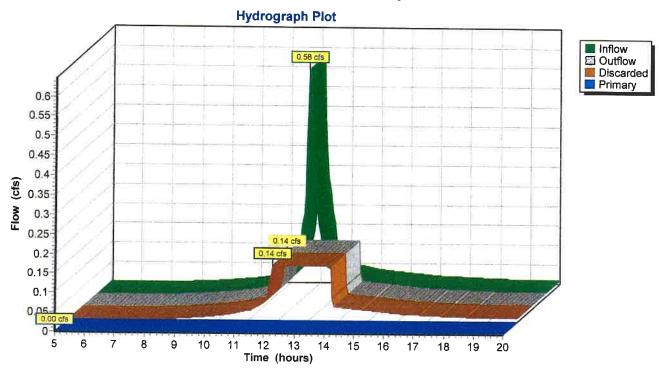
# **Discarded OutFlow** (Free Discharge) 2=Exfiltration

# Primary OutFlow (Free Discharge) 1=Broad-Crested Rectangular Weir

#_	Routing	Invert	Outlet Devices
1	Primary		12.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32
2	Discarded	74.30'	0.14 cfs Exfiltration when above invert

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# Pond P-1: Infiltration System



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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Type III 24-hr Rainfall=6.35" Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment B-1: Tributary to Street

Tc=5.0 min CN=56 Area=6,839 sf Runoff= 0.31 cfs 0.021 af

Subcatchment B-2: Tributary to Infiltration

Tc=5.0 min CN=81 Area=6,857 sf Runoff= 0.77 cfs 0.052 af

Reach R-1: Summary Node

Inflow= 0.31 cfs 0.021 af

Outflow= 0.31 cfs 0.021 af

Pond P-1: Infiltration System

Peak Storage= 644 cf Inflow= 0.77 cfs 0.052 af

Discarded= 0.14 cfs 0.052 af Primary= 0.00 cfs 0.000 af Outflow= 0.14 cfs 0.052 af

Runoff Area = 0.314 ac Volume = 0.073 af Average Depth = 2.80"

Page 14 5/30/2023

### **Subcatchment B-1: Tributary to Street**

Runoff

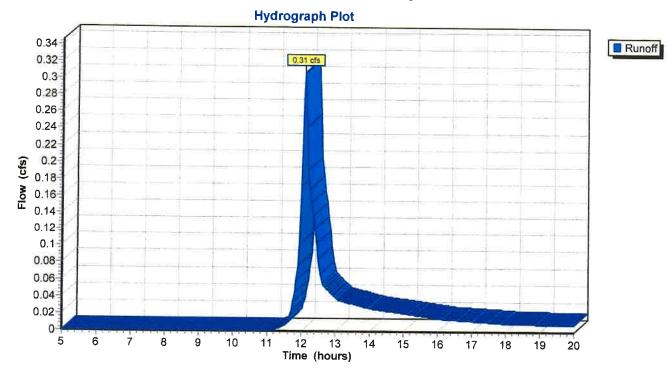
0.31 cfs @ 12.09 hrs, Volume=

0.021 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=6.35"

A	rea (sf)	CN	Description						
	1,952	98	Paved parking & roofs						
	4,887	39	>75% Grass cover, Good, HSG A						
	6,839 56 Weighted Average								
Tc (min)	Length (feet)	Slope (ft/ft	- 7	Capacity (cfs)	Description				
5.0					Direct Entry, Overland Flow				

### **Subcatchment B-1: Tributary to Street**



Page 15

5/30/2023

# Subcatchment B-2: Tributary to Infiltration

Runoff

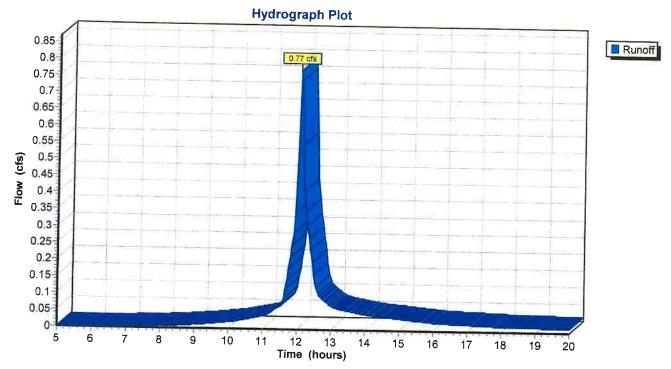
0.77 cfs @ 12.07 hrs, Volume=

0.052 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=6.35"

A	rea (sf)	CN	Description							
	4,876	98	Paved parking & roofs							
	1,981	39	9 >75% Grass cover, Good, HSG A							
	6,857	81 Weighted Average								
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description					
5.0					Direct Entry, Overland Flow					

# Subcatchment B-2: Tributary to Infiltration



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Page 16 5/30/2023

## Reach R-1: Summary Node

Inflow

0.31 cfs @ 12.09 hrs, Volume=

0.021 af

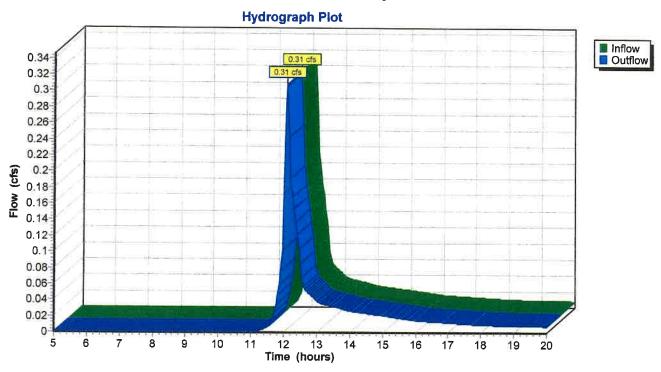
Outflow

0.31 cfs @ 12.09 hrs, Volume=

0.021 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

## Reach R-1: Summary Node



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Page 17 5/30/2023

## Pond P-1: Infiltration System

Inflow	=	0.77 cfs @	12.07 hrs,	Volume=	0.052 af		
- 0.1., - 1.	=	0.14 cfs @	11.75 hrs.			Atten= 82%	Lag= 0.0 min
Discarded	=	0.14 cfs @	11.75 hrs,	Volume=	0.052 af	7 ttto11- 02 70,	Lag- 0.0 mm
Primary	=	0.00 cfs @	5.00 hrs,	Volume=	0.000 af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 77.41' Storage= 644 cf

Plug-Flow detention time= 29.2 min calculated for 0.052 af (100% of inflow)

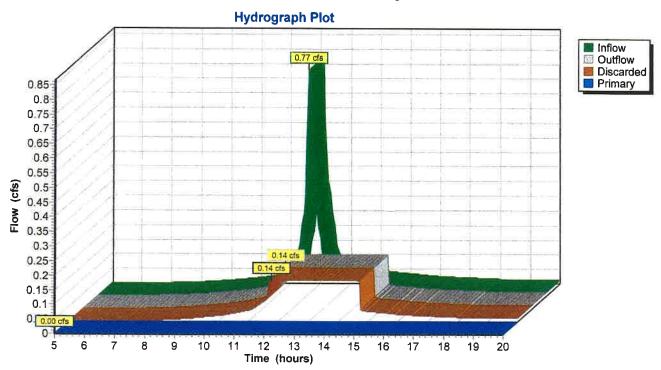
Elevation	Cum.Store
(feet)	(cubic-feet)
74.30	0
74.80	126
75.97	540
76.47	591
77.60	655

## **Discarded OutFlow** (Free Discharge) 2=Exfiltration

## Primary OutFlow (Free Discharge) 1=Broad-Crested Rectangular Weir

#_	Routing	Invert	Outlet Devices
1	Primary	77.50'	12.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00
2	Discarded		Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 <b>0.14 cfs Exfiltration when above invert</b>

**Pond P-1: Infiltration System** 



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Page 19 5/30/2023

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Type III 24-hr Rainfall=8.78"
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment B-1: Tributary to Street

Tc=5.0 min CN=56 Area=6,839 sf Runoff= 0.62 cfs 0.042 af

Subcatchment B-2: Tributary to Infiltration

Tc=5.0 min CN=81 Area=6,857 sf Runoff= 1.17 cfs 0.080 af

Reach R-1: Summary Node

Inflow= 1.99 cfs 0.055 af

Outflow= 1.99 cfs 0.055 af

Pond P-1: Infiltration System

Peak Storage= 657 cf Inflow= 1.17 cfs 0.080 af

Discarded= 0.14 cfs 0.067 af Primary= 1.51 cfs 0.013 af Outflow= 1.65 cfs 0.080 af

Runoff Area = 0.314 ac Volume = 0.122 af Average Depth = 4.65"

Page 20

5/30/2023

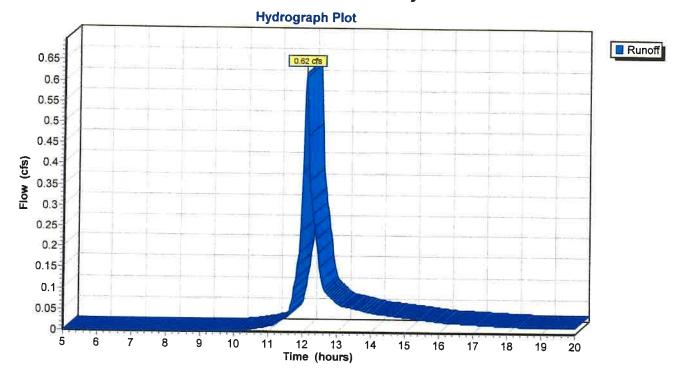
## **Subcatchment B-1: Tributary to Street**

0.62 cfs @ 12.08 hrs, Volume= Runoff 0.042 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=8.78"

A	rea (sf)	CN	Description			
	1,952 4,887		Paved park >75% Gras		ood, HSG A	
	6,839		Weighted A		754, 1100 /1	
Tc (min)	Length (feet)	Slope (ft/ft)	40.00 mg/s	Capacity (cfs)	Description	
5.0					Direct Entry, Overland Flow	

## Subcatchment B-1: Tributary to Street



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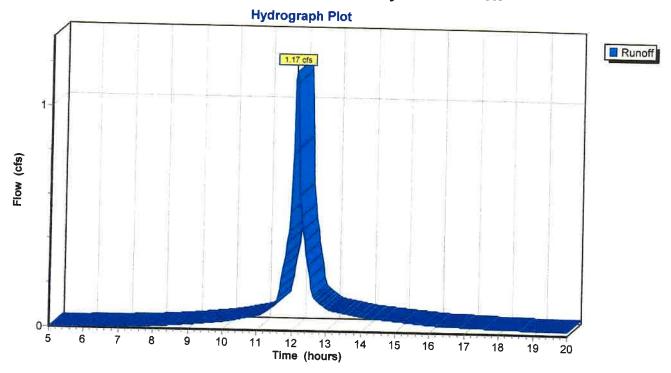
## Subcatchment B-2: Tributary to Infiltration

Runoff 1.17 cfs @ 12.07 hrs, Volume= 0.080 af

Runoff by SCS TR-20 method, UH=SCS, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr Rainfall=8.78"

A	rea (sf)	CN	Description			
	4,876 1,981	98 39	Paved park >75% Gras	ing & roofs s cover. Go	pod, HSG A	
	6,857		Weighted A		, 1100 A	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
5.0					Direct Entry, Overland Flow	

## Subcatchment B-2: Tributary to Infiltration



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Page 22

5/30/2023

## Reach R-1: Summary Node

Inflow =

1.99 cfs @ 12.15 hrs, Volume=

0.055 af

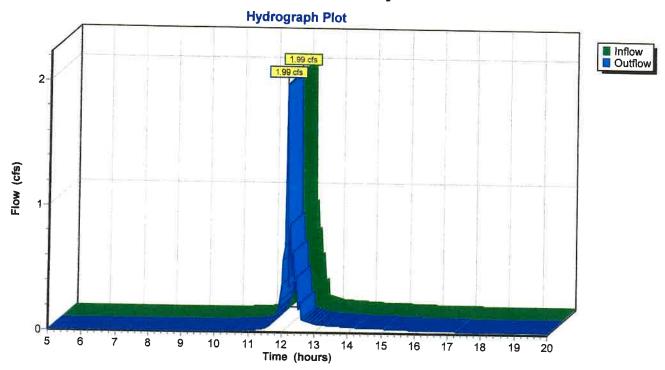
Outflow

1.99 cfs @ 12.15 hrs, Volume=

0.055 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

## Reach R-1: Summary Node



Page 23

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5/30/2023

## Pond P-1: Infiltration System

Inflow Outflow Discarded Primary	=	1.17 cfs @ 1.65 cfs @ 0.14 cfs @ 1.51 cfs @	12.15 hrs, 11.65 hrs,	Volume= Volume=	0.080 af 0.080 af, 0.067 af 0.013 af	Atten= 0%,	Lag= 4.6 min
---	---	--	--------------------------	--------------------	---	------------	--------------

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 77.64' Storage= 657 cf

Plug-Flow detention time= 26.1 min calculated for 0.080 af (100% of inflow)

Cum.Store
(cubic-feet)
0
126
540
591
655

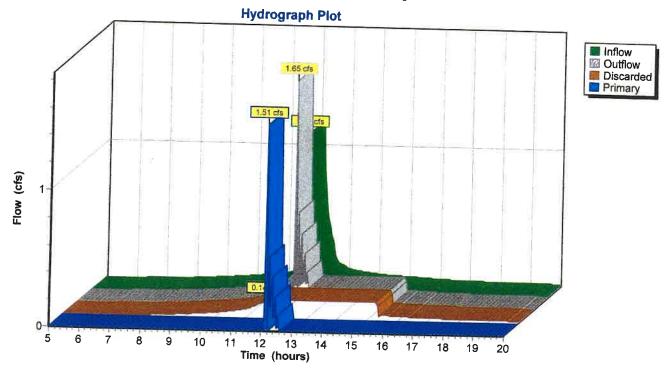
## **Discarded OutFlow** (Free Discharge) 2=Exfiltration

## Primary OutFlow (Free Discharge) 1=Broad-Crested Rectangular Weir

#_	Routing	Invert	Outlet Devices
1	Primary	77.50'	12.0' long x 1.0' breadth Broad-Crested Rectangular Weir
2	Discarded		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 0.14 cfs Exfiltration when above invert

5/30/2023

Pond P-1: Infiltration System



## OPERATION & MAINTENANCE PLAN STORMWATER MANAGEMENT FACILITIES 2202 COMMONWEALTH AVENUE NEWTON, MASSACHUSETTS



June 2, 2023

Lakeview Engineering Associates P.O. Box 787 Hudson, Massachusetts 01749

## OPERATION & MAINTENANCE PLAN STORMWATER MANAGEMENT FACILITIES 2202 COMMONWEALTH AVENUE NEWTON, MASSACHUSETTS

The proposed project includes stormwater runoff controls associated with the redevelopment of the existing house lot to a multi-family use, including a new building layout, access driveway & site grading, that will require continued maintenance by the property owner. The major components associated with maintenance needs is are the trench drain, sediment trap manhole, the leaching galley system & the yard drain, as well as the roof gutters & downspouts. These will need to be cleaned periodically as noted below. Cleaning of these structures shall be done by the property owner or by a specialty contractor with hydraulic cleaning ability. The following outlines the major maintenance issues associated with the project:

## Trench Drain Cleaning:

The trench drain should be inspected after completion of construction to assure that all debris was removed and no construction material will be cause the system to clog or restrict the outlet.

Maintenance of this system is subject to continuous monitoring after storm events to determine frequency of maintenance needs. The trench drain should be cleaned manually, after all major storms or as a minimum, once per month to remove accumulated solids and debris. This is required to prevent clogging and overflow of solids to the driveway. Assuming the trench drains are maintained and cleaning is routinely performed, the driveway runoff and associated solids should be routed to the sediment trap for removal, prior to infiltration.

## Sediment Trap Manhole:

The sediment trap manhole should be inspected after completion of construction to assure that all debris was removed and no construction material will be cause the system to clog.

Maintenance of this system is subject to on-site evaluation and catchbasin type maintenance. Initially, this system should be inspected on a monthly / storm event schedule to note any solids carry over. After the first year of operation, the system should receive quarterly inspections. It is recommended that the sediment trap manhole should be cleaned at least twice yearly (Spring & Fall).

## **Galley Infiltration System:**

The galley infiltration system should be inspected after completion of construction to assure that all debris was removed and no construction material will be cause the system to clog.

The proposed system are intended to be used for collection & storage of roof and driveway runoff, for infiltration after a storm event. As part of this process, some soil and debris could collect in these galleys. This should be removed periodically, every four to five years, to maximize infiltration and storage capabilities. The debris / soil must be removed by means of hydraulic vacuuming by a specialty contractor.

## Yard Drain:

The yard drain manhole should be inspected after completion of construction to assure that all debris was removed and no construction material will be cause the system to clog.

Maintenance of this system is subject to on-site evaluation and catchbasin type maintenance. Initially, this system should be inspected on a monthly / storm event schedule to note any solids carry over. After the first year of operation, the system should receive quarterly inspections. It is recommended that the yard drain manhole should be cleaned at least twice yearly (Spring & Fall).

## **Gutters & Downspouts Cleaning:**

The roof gutters & downspouts should be inspected after completion of construction to assure that all debris was removed and no construction material will be cause the system to clog or restrict the outlet.

Maintenance of the gutter system should be performed at least twice a year (Spring & Fall) to assure the gutters & downspouts are functional.

## **Galley Infiltration System:**

The galley infiltration system should be inspected after completion of construction to assure that all debris was removed and no construction material will be cause the system to clog.

The proposed systems are intended to be used for collection & storage of roof and driveway runoff, for infiltration after a storm event. As part of this process, some soil and debris could collect in these galleys. This should be removed periodically, every four to five years, to maximize infiltration and storage capabilities. The debris / soil must be removed by means of hydraulic vacuuming by a specialty contractor.

## Maintenance Responsibilities

The maintenance of the various drainage system components is the responsibility of the Property Owner (Condominium Association). Some of the work (gutters) can be accomplished by the Owner or a landscape contractor. The infiltration system be contracted to a company that specializes in the cleaning of storm drainage facilities. Inspections should be performed by independent individual such as the design engineer or other experienced individual in the field.

## STORMWATER MANAGEMENT REPORT 2202 COMMONWEALTH AVENUE NEWTON, MASSACHUSETTS

## **INSPECTION REPORT:**

Inspection Firm:	
Inspectors Name:	Date:
Components Inspected:	
SYSTEM MAINTENANCE:	
Maintenance Firm:	Date :
Gutters & Downspouts Inspected: Yes	No Comments:
Gutters & Downspouts Cleaned: Yes	No Comments:
Trench Drain Inspected: Yes No	Comments:
Trench Drain Cleaned: Yes No	Comments:
Sediment Trap Manhole Inspected: Yes _	No Comments:
Sediment Trap Manhole Cleaned: Yes	_No Comments:

g Galleys Cleaned: Yes No Comments:  ain Inspected: Yes No Comments:  in Cleaned: Yes No Comments:
nin Inspected: Yes No Comments:
of Material Removed:
nments:
r

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Page 1 5/30/2023

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Type III 24-hr Rainfall=2.00"
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment B-1: Tributary to Street** 

Tc=5.0 min CN=56 Area=6,839 sf Runoff= 0.00 cfs 0.000 af

Subcatchment B-2: Tributary to Infiltration

Tc=5.0 min CN=81 Area=6,857 sf Runoff= 0.10 cfs 0.007 af

Reach R-1: Summary Node

Inflow= 0.00 cfs 0.000 af Outflow= 0.00 cfs 0.000 af

Pond P-1: Infiltration System

Peak Storage= 6 cf Inflow= 0.10 cfs 0.007 af

Discarded= 0.10 cfs 0.007 af Primary= 0.00 cfs 0.000 af Outflow= 0.10 cfs 0.007 af

Runoff Area = 0.314 ac Volume = 0.007 af Average Depth = 0.28"

## Commonwealth of Massachusetts City/Town of

# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

Form 11 – Soil Suitability Assessment for On-Site Sewage Disposal • Page 1 of 8



## Commonwealth of Massachusetts City/Town of Newton

# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

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Form 11 – Soil Suitability Assessment for On-Site Sewage Disposal • Page 2 of 8

## Commonwealth of Massachusetts City/Town of Newton

# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

## C. On-Site Review (continued)

Deep Observation Hole Number:

DH-1

T.5 YE 2/2         Color         Percent         (USDA)         Gravel Stones         Spoile Structure Stones         Structure Stones         Spoile Structure Stones         Spoile Structure Stones         Spoile Structure Stones         Spoile Structure Stones         Copy Structure Stones         Massive Structure Stones         Massive Structure Stru	A         7.5 YE 2/2         Color         Percent         (USDA)         Gravel         Cobbles & Stones         Structure (Moist)           B         7.5 YR 5/8         102"         10 YR         >5%         Sandy         Assive         Dry           C1         2.5 Y 5/1         102"         5/6         >5%         Sandy         5%         20%         Single Dry           C2         2.5 Y 5/1         Sandy         5%         20%         Massive         Dry           C2         2.5 Y 5/1         Sandy         5%         20%         Massive         Dry	Depth (in.)	Soil Horizon/	Depth (in.) Soil Horizon/Soil Matrix: Color-	Redox	Redoximorphic Features (mottles)		Soil Texture	1	Coarse Fragments % by Volume		io	
A         7.5 YE 2/2         Sandy Loam Loam Loam Loam         Sandy Loam Loam Loam         Massive Bry Grain         Dry Grain           C1         2.5 Y 6/3         102" 5/6         >5%         Sandy Loam Sandy Sand Sand Grain         25%         20%         Massive Massive Damp           C2         2.5 Y 5/1         Sandy Sandy Sandy Sandy Loam Loam         5%         20%         Massive Massive Damp	A         7.5 YE 2/2         Sandy Loam         Sandy Loam         Massive         Dry           B         7.5 YR 5/8         102" 10 YR 5/6         >5%         Sandy Loam         Massive         Dry           C1         2.5 Y 6/3         102" 5/6         >5%         Sandy Grain         Dry           C2         2.5 Y 5/1         Sandy Loam         5%         20%         Massive         Damp           C3         2.5 Y 5/1         Loam         5%         20%         Massive         Damp		Layer	Moist (Munsell)	Depth	Color		(USDA)	Gre	Cobbles &		Consistence (Moist)	
B 7.5 YR 5/8 Sandy Sandy Loam Sandy Loam Sandy Loam Sandy Loam Loam 10 YR >5% Sand 25% 20% Grain Dry C2 2.5 Y 5/1 Sandy Loam 5% 20% Massive Damp Loam Loam 5% 20% Massive Damp	B   7.5 YR 5/8   Sandy   Loam   Massive   Dry   Sandy   Loam   Loam   Massive   Dry   Loam   Loam   Sandy   25%   20%   Single   Dry   C2   2.5 Y 5/1   Sandy   5%   20%   Massive   Damp   Loam   5%   20%   Massive   Damp   C4   C5 Y 5/1   C6   C6   C6   C7   C6   C7   C7   C7	18	۵	7 5 VE 2/0				Condy		Stones			
B         7.5 YR 5/8         Sandy Loam         Sandy Loam         Massive Dry Grain         Dry Grain           C1         2.5 Y 6/3         102" 5/6         >5%         Sand 25%         20%         Single Grain         Dry Grain           C2         2.5 Y 5/1         Sandy Loam         5%         20%         Massive Damp	B         7.5 YR 5/8         Sandy Loam         Sandy Loam         Massive Dry Grain         Dry Grain           C1         2.5 Y 6/3         102" 5/6         >5%         Sandy Grain         Dry Grain         Dry Grain           C2         2.5 Y 5/1         Loam         Sandy Loam         5%         20%         Massive Damp			1.3 15 2/2				Loam			Massive	Drv	Fine
C1 2.5 Y 6/3 102" 10 YR >5% Sand 25% 20% Single Dry C2 2.5 Y 5/1 Sandy 5% 20% Massive Damp Loam 5% 20% Massive Damp	C1 2.5 Y 6/3 102" 10 YR >5% Sand 25% 20% Single Dry C2 2.5 Y 5/1 Sandy 5% 20% Massive Damp Loam 5% 20% Massive Damp	40,,	8	7.5 YR 5/8				Sandy					
C2 2.5 Y 6/3 102" 10 YR >5% Sand 25% 20% Single Dry C2 2.5 Y 5/1 Sandy 5% 20% Massive Damp	C2 2.5 Y 6/3 102" 10 YR >5% Sand 25% 20% Single Dry C2 2.5 Y 5/1							Loam			Massive	Drv	Fi
C2 2.5 Y 5/1 Sandy 5% 20% Grain Dry Loam Loam 5% 20% Massive Damp	C2 2.5 Y 5/1 Sandy 25% 20% Grain Dry Grain Loam 5% 20% Massive Damp	102"	5	25 7 673	1007	10 YR							2
C2 2.5 Y 5/1 Sandy 5% 20% Massive Damp	C2 2.5 Y 5/1 Sandy 5% 20% Massive Damp		5	2.0 1 0/3	102"	5/6	>5%	Sand	72%	20%	Single		Coarse,
Loam 5% 20% Massive Damp	Loam 5% 20% Massive Damp	114"	S	25 7 7 7 7				Condi			Grain		Compact
			70	1/0 1 0.7				Loam	2%	20%	Massive		Medium,
					ř.							- /	Compact

Additional Notes:





## Commonwealth of Massachusetts

City/Town of Newton

# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

	Fair Weather	See Site plan	Surface Stones See Site Plan	Position on Landscape (attach sheet) <100 Possible Wet Area < 100	<pre>c100 feet feet feet</pre>	⊠ Yes	☐ Weathered/Fractured Rock	N/A Depth Weeping from Pit Depth Standing Water in Hole
	DH-2 12/22/22 AM Date Time	82.0+/- Location (identify on plan):	Kame Terrace Landform	<100 Crainage Way	10' feet Drinking Water Well			If yes: N/A 114" 72.5+/- Depth v inches elevation
C. On-Site Review (continued)	Deep Observation Hole Number: 1. Location	Ground Elevation at Surface of Hole:  2. Land Use Residential Action (e.g., woodland arrivelless)	Pavement Vegetation	3. Distances from: Open Water Body	Property Line  4. Parent Material: Glacial Outwash	Disturbed Soit	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	Grot

Form 11 – Soil Suitability Assessment for On-Site Sewage Disposal • Page 4 of 8

## Form 11 – Soil Suitability Assessment for On-Site Sewage Disposal • Page 5 of 8

## Commonwealth of Massachusetts City/Town of Newton

# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

## C. On-Site Review (continued)

Deep Observation Hole Number:

DH.3

number of the line	Depth (in.)	Soil Horizon/	Depth (in.) Soil Horizon/Soil Matrix: Color-		Redoximorphic Features (mottles)	eatures	Soil Texture		Coarse Fragments	110	:	
Pavement         N/A         Driveway         Sandy         A C.5 YR 2/2         Came of the control of		i i	moist (munsell)	Depth	Color	Percent	(USDA)	Gravet	Cobbles &	Structur	Consistence	Other
A         7.5 YR 2/2         Sandy Loam         Loam         Massive         Dry           B         7.5 YR 5/8         Sandy Loam         Massive         Dry           C1         2.5 Y 5/2         Sandy Loam         5%         10%         Massive         Dry           C2         2.5 Y 5/3         Sand         25%         20%         Single Grain         Dry	2"	Pavement	N/A						Stones		(IMOIST)	
A         7.5 YR 5/2         Sandy Loam         Massive         Dry           C1         2.5 Y 5/2         Sandy Loam         5%         10%         Massive         Dry           C2         2.5 Y 5/3         Sandy Loam         5%         10%         Massive         Dry           C2         2.5 Y 5/3         Sand         25%         20%         Single Grain         Dry	12"	<					Uriveway					
B         7.5 YR 5/8         Loam         Massive         Dry           C1         2.5 Y 5/2         Sandy         5%         10%         Massive         Dry           C2         2.5 Y 5/3         Sandy         5%         10%         Massive         Dry           Sand         25%         20%         Single         Dry	7.	τ	7.5 YR 2/2				Sandy			:		
C1 2.5 Y 5/2 Loam Massive Dry Sandy Loam Massive Dry Sandy 5% 10% Massive Dry C2 2.5 Y 5/3 Sand 25% 20% Single Dry Grain Dry	"PC	٥	1				Loam			Massive	Dry	Fine
C1 2.5 Y 5/2 Sandy Sandy 5% 10% Massive Dry Loam Sand 25% 20% Single Dry Grain Dry	1	۵	7.5 YR 5/8				Sandy		S.			
C2 2.5 Y 5/2 Loam 5% 10% Massive Dry C2 2.5 Y 5/3 Sand 25% 20% Single Dry Grain Dry		5					Loam			Massive	Dry	Fine
C2 2.5 Y 5/3	2	5	2.5 Y 5/2				Sandy	50%	400,	4 4		Modi
Sand 25% 20% Single Dry Grain	114"	S	25 8 613				Loam	2	801	Massive	Dry	Compact
			25				Sand	25%	20%	Single Grain	Dry	Coarse.
												200

Additional Notes:



## Commonwealth of Massachusetts

# City/Town of Newton Form 11 - Soil Suitability

 D. Determination of High Groundwater Elevation	Method Used:	☐ Depth observed standing water in observation hole A.	Depth weeping from side of observation hole A.	Depth to soil redoximorphic features (mottles)  A. 102"	inches A.		Adjustment Factor Adjusted Groundwater Level	E. Depth of Pervious Material	Depth of Naturally Occurring Pervious Material	Does at least four feet of naturally occurring pervious material exist in all areas observed throughout the area property.	No	If yes, at what depth was it observed?  Upper boundary: 40"  Inches Lower boundary: inches
D. D	1. Me		$\boxtimes$		2.	O.E.	Adjus	E. Dep	. Depth	e, D g	XI	<u>ج</u> م
					. •							



## Commonwealth of Massachusetts

City/Town of Newton

# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

## F. Certification

described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.100 through 15.107. evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct soil

Date of Soil Evaluator Exam Board of Health July 1995 12/27/22 ۷X Typed or Printed Name of Soil Evaluator / License # Name of Board of Health Witness Stephen E. Poole SE1955 Signature of Soil Evaluator None

**Note:** In accordance with 310 CMR 15.018(2) this form must be submitted to the approving authority within 60 days of the date of field testing, and to the designer and the property owner with <u>Percolation Test Form 12.</u>

Form 11 – Soil Suitability Assessment for On-Site Sewage Disposal • Page 7 of 8

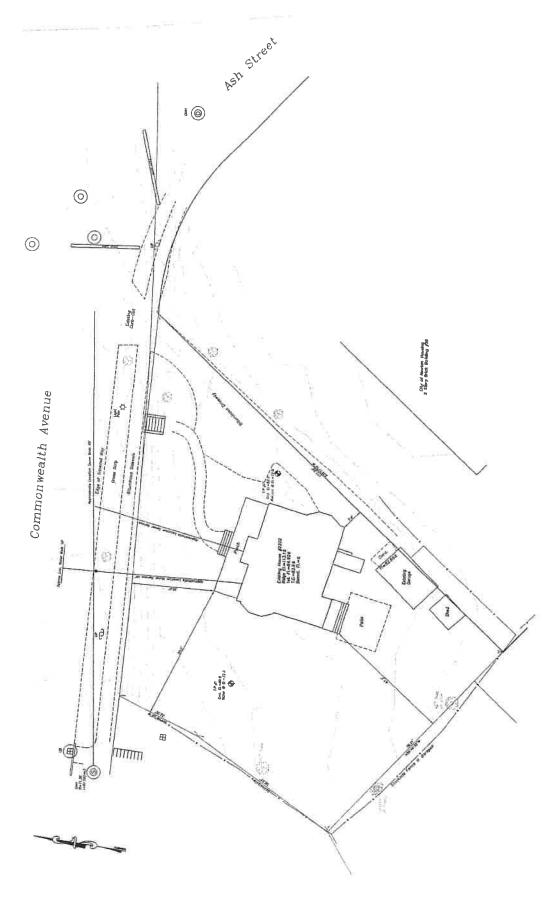
## Form 11 – Soil Suitability Assessment for On-Site Sewage Disposal • Page 8 of 8

## Commonwealth of Massachusetts City/Town of Newton

# Form 11 - Soil Suitability Assessment for On-Site Sewage Disposal

## Field Diagrams

Use this sheet for field diagrams:







## Commonwealth of Massachusetts City/Town of

## **Percolation Test**

Form 12

Percolation test results must be submitted with the Soil Suitability Assessment for On-site Sewage Disposal. DEP has provided this form for use by local Boards of Health. Other forms may be used, but the local Board of Health to determine the form they use.

A. Site Information

Important:
When filling out
forms on the
computer, use
only the tab key
to move your
cursor - do not
use the return
key.





2202 Commonwealth Avenu	ie, LLC			
Owner Marine				
2202 Commonwealth Avenu Street Address or Lot #	<u>e</u>			
Newton				
City/Town		MA	0246	6-1804
Cost		State	Zip Co	ode
Contact Person (if different from Ow	ner)	Telephone Nun	nher	
B. Test Results		- Inches Hall		
	12/22/22	09:35 AM	10/00/00	
	Date	Time	12/22/22 Date	10:05 AM
Observation Hole#	#1 (P-1)		#2 (P-2)	Time
Depth of Perc	56" (76.1)		65" (76.6)	
Start Pre-Soak	09:35 AM		10:05 AM	
End Pre-Soak	09:48 AM		10:19 AM	
Time at 12"				
Time at 9"		-		
Time at 6"				
Time (9"-6")	<15 Min.		<15 Min.	
Rate (Min./Inch)	2 MPI		2 MPI	
Stephen E. Poole, SE 1955 Test Performed By:	Test Passed: Test Failed:		Test Passed: Test Failed:	
Witnessed By:				
Comments:				
very Stony Gravel, Somewhat C	Compact			
Very Stony Gravel, Somewhat C	Compact			



**MAP LEGEND** 

Area of Ir	Area of Interest (AOI)	4	Spoil Area
	Area of Interest (AOI)	U	Baltings
Soils		•	Stony Spot
	Soil Map Unit Polygons		Very Stony Spot
1	Soil Map Unit Lines	(E)	Wet Spot
2:	Soil Map Unit Points	9	Other
Special	Special Point Features	ţ	Special Line Features
9	Blowout	Water Features	itures
Ø	Borrow Pit		Streams and Canals
滩	Clay Spot	Transportation	ation
{ <		ŧ	Rails
<b>\( \)</b>	Closed Depression	}	Inferstate Highways
Æ	Gravel Pit		IIS Routes
• 7	Gravelly Spot		Source of the second of the se
0	Landfill		Major Koads
æ	Lava Flow		Local Roads
ć		Background	P
#	Marsh or swamp		Aerial Photography
*	Mine or Quarry		
0	Miscellaneous Water		
•			

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:25,000.

Waming: Soil Map may not be valid at this scale.

contrasting soils that could have been shown at a more detailed misunderstanding of the detail of mapping and accuracy of soil Enlargement of maps beyond the scale of mapping can cause line placement. The maps do not show the small areas of

Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Middlesex County, Massachusetts Survey Area Data: Version 22, Sep 9, 2022 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: May 22, 2022-Jun 5, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Severely Eroded Spot

Slide or Slip Sodic Spot

Sinkhole

Perennial Water Rock Outcrop

Saline Spot Sandy Spot

## **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
626B	Merrimac-Urban land complex, 0 to 8 percent slopes	3.1	58.09
656	Udorthents-Urban land complex	2.2	42.0%
Totals for Area of Interest		5.3	100.0%

## Middlesex County, Massachusetts

## 626B—Merrimac-Urban land complex, 0 to 8 percent slopes

## Map Unit Setting

National map unit symbol: 2tyr9

Elevation: 0 to 820 feet

Mean annual precipitation: 36 to 71 inches

Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Merrimac and similar soils: 45 percent

Urban land: 40 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

## **Description of Merrimac**

## Setting

Landform: Outwash plains, outwash terraces, moraines, eskers,

Landform position (two-dimensional): Summit, shoulder, backslope,

footslope

Landform position (three-dimensional): Crest, side slope, riser,

tread

Down-slope shape: Convex

Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite,

schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite, schist, and gneiss

## Typical profile

Ap - 0 to 10 inches: fine sandy loam

Bw1 - 10 to 22 inches: fine sandy loam

Bw2 - 22 to 26 inches: stratified gravel to gravelly loamy sand 2C - 26 to 65 inches: stratified gravel to very gravelly sand

## Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water

(Ksat): Moderately high to very high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 2 percent Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)

Sodium adsorption ratio, maximum: 1.0 Available water supply, 0 to 60 inches: Low (about 4.6 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

## **Description of Urban Land**

## Typical profile

M - 0 to 10 inches: cemented material

## Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: 0 inches to manufactured layer

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low

(0.00 to 0.00 in/hr)

Available water supply, 0 to 60 inches: Very low (about 0.0 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D Hydric soil rating: Unranked

## **Minor Components**

## Windsor

Percent of map unit: 5 percent

Landform: Outwash terraces, dunes, outwash plains, deltas

Landform position (three-dimensional): Tread, riser

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

## Sudbury

Percent of map unit: 5 percent

Landform: Deltas, terraces, outwash plains Landform position (two-dimensional): Footslope Landform position (three-dimensional). Tread, dip

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

## Hinckley

Percent of map unit: 5 percent

Landform: Deltas, kames, eskers, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Head slope, nose slope,

crest, side slope, rise Down-slope shape: Convex

Across-slope shape: Convex, linear Hydric soil rating: No

## **Data Source Information**

Soil Survey Area: Middlesex County, Massachusetts

Survey Area Data: Version 22, Sep 9, 2022

## POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

## PF tabular

Durati	S-based p			Averac	le recurren	1.761, 30	/o Comma	ence inter	rvals (in i	nches)1
	1	2	5	10	e recurren	e unalivai	(years)			
5-mir	0.301 (0.241-0.37)	0.372 7) (0.298-0.46)	0.488	0.585	0.718	0.817	0.924	200	500	1000
10-mii	0.427	0.528	0.602	0.830	1.02	1.16	1.31	3) (0.711-1.55 1.49	(0.803-1.90	(0.881-2.
15-mii	0.000	0.621	0.815	0.976	1.20	1.36	0) (0.949-1.8	9) (1.01-2.19	1.75 (1.14-2.69) 2.06	
30-mlr		0.849	1.12	1.34	1.64	1.87			(1.34-3.16)	
60-min	0.000	1.08	1.42	(1.06-1.70)	(1.25-2.20)	{1.40-2.58		) (1.63-3.54)	(1100)	3.21 (2.03-5.0
2-hr	1.12	1.40	(1.13-1.78) 1.85	(1.34-2.15)	(1.60-2.80)	(1.78-3,27	) (1.95-3.88	3.05 (2.07-4.50)	3.62 (2.35-5.56)	4.10 (2.59-6.4
3-hr	(0.905-1.40)	(1.13-1.74) 1.63	(1.48-2.31)	(1.77-2.80)	(2.11-3.66)	3.11 (2.35-4.28	3.53 (2.59-5.10)	<b>4.04</b> (2.75-5.91)	4.84 (3.15-7.37)	5.54 (3.52-8.6
6-hr	(1.06-1.62) 1.70	(1.32-2.02) <b>2.11</b>	(1.73-2.68)	(2.07-3.24)	3.18 (2.46-4.24)	3.62 (2.74-4.96)	<b>4.10</b> (3.02-5,91)	4.71 (3.21-6.85)	<b>5.66</b> (3.69-8.56)	6.48 (4.12-10.0
-	(1.39-2.10)	(1.71-2.60)	(2.24-3.43)	3.31 (2.66-4.13)	4.07 (3.16-5.37)	4.62 (3.52-6.28)	5.23 (3.87-7.46)	5.99 (4.10-8,63)	7.16 (4.69-10.7)	8.19 (5.22-12.5
12-hr	(1.79-2.68)	(2.20-3.30)	3.50 (2.86-4.31)	4.18 (3.38-5.18)	5.11 (3.99-6.69)	5.80 (4.43-7.79)	6.55 (4.85-9.22)	7.46 (5.12-10.6)	8.85 (5.82-13.1)	10.1
24-hr	2.66 (2.19-3.23)	<b>3.29</b> (2.71-4.00)	4.32 (3.54-5,28)	5.17 (4.21-6.36)	<b>6.35</b> (4.99-8.25)	7.21 (5.54-9,63)	8.16 (6.08-11.4)	9.33	11.1	(6.44-15.2 12.7
2-day	3.05 (2.53-3.68)	3.84 (3.18-4.65)	5.14 (4.24-6.25)	6.22 (5.10-7.60)	7.71 (6.10-9.99)	8.79	10.00	(6.43-13.2)	(7.34-18.4) 14.0	(8.16-19.1 16.2
3-day	3.36 (2.79-4.04)	<b>4.22</b> (3.51-5.08)	5.63 (4.66-6.80)	6.79 (5.59-8.27)	8.40 (6.68-10.8)	9.57	(7.53-14.0) 10.9	(7.99-16.2) 12.6	(9.27-20.4) 15.3	17.8
1-day	3.64 (3.04-4.37)	4.53 (3.78-5.45)	5.99 (4.97-7.22)	7.20	8.86	(7.45-12.7) 10.1	(8.24-15.2) 11.4	(8.72-17.6) 13.2	(10.1-22,2) 16,0	18.6
-day	4.41 (3.70-5.27)	5.34 (4.47-6.38)	6.86 (5.72-8.22)	(5.93-8.73) 8.12	9.85	(7.86-13.3) 11.1	(8.67-15.9) 12.5	(9.16-18.3) 14.3		(12.0-27.3) 19.9
0-day	5.13	6.08 (5.11-7.24)	7.63	8.92	(7.88-12.6) 10.7	(8.69-14.6) 12.0	(9.51-17.2) 13.4	(9.99-19.8) <b>15.3</b>		(12.9-29.0) 20.6
)-day	7.19	8.21	9.89	11.3	13.2	(9.39-15.6) 14.6	(10.2-18.3)	0. 27	III	13.4-29.9)
-day	8.88	9.96	11.7	13.2	15.2	(11.4-18.6) 16.8	Sec. 1 2 1 13		(13.7-28.7)	22.5 14.6-32.3)
-day	11.0	12.1	14.0	(11.1-15.7) 15.5	(12.2-18.8) 17.7	(13.1-21.1)	(13.7-23.9)	(14.1-26.9)	THE RESERVE OF STREET, SALES	24.0 15.6-34.2)
-day	12.8	13.9	(11.9-16.5) ( 15.9		(14.2-21.6)	15.1-24.1)	(15.6-26.9)	(16.0-30.1)		<b>26.0</b> (6.9-36.8)
-day	12.8	13.9	(11.9-16.5) ( 15.9	13.1-18.4) ( 17.5	14.2-21.6) ( 19.7	21.4	23.1	24.6	24.5 16.6-34.0) (1 26.5 17.9-36.5) (1	16

Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Back to Top

PF graphical