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<u>PRINCIPALS</u> Robert J. Michaud, P.E. Ronald D. Desrosiers, P.E., PTOE Daniel J. Mills, P.E., PTOE

No

MEMORANDUM

DATE: September 5, 2019

TO: Paul Capasso Packard Cove Associates LLP 49 Lexington Street Newton, MA 02465

FROM: Robert J. Michaud, P.E. – Managing Principal Daniel A. Dumais, P.E. – Senior Project Manager

RE: Proposed Residential Development 15 & 21 Lexington Street – Newton, MA

MDM Transportation Consultants, Inc. (MDM) has prepared this traffic impact assessment (TIA) for the proposed apartment development to be located at 15 & 21 Lexington Street in Newton, Massachusetts. The location of the site relative to adjacent roadways is shown in **Figure 1**. This memorandum describes existing (baseline) traffic conditions for adjacent roadways, trip generation characteristics of the proposed development, quantifies incremental traffic impacts of the Site development on area roadways, and evaluates safety-related conditions at key study locations that provide access to the Site. Several improvements aimed at enhancing traffic operations and/or safety is outlined under *Recommendations and Conclusions*.

Key findings of the traffic assessment are as follows:

- *Baseline Traffic Volumes.* Lexington Street carries approximately 15,010 vehicles per day (vpd) on weekdays. Peak hour traffic flow on Lexington Street is approximately 7 to 8 percent of the daily flow with directional flow generally evenly distributed between the northbound and southbound directions.
- □ *Safety Characteristics*. A review of MassDOT crash data indicates that no immediate safety countermeasures are warranted based on the crash history at the study intersections. Likewise, the available sight lines at the proposed Site Driveway intersection with Lexington Street will exceed the minimum and ideal sight line requirements from AASHTO.

Traffic Impact Assessment Newton, Massachusetts



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Site Location

- □ *Modest Trip Generation*. The proposed development is estimated to generate approximately 11 vehicle trips (3 entering and 8 exiting) during the weekday morning peak hour and 13 vehicle trips (8 entering and 5 exiting) during the weekday evening peak hour. On a daily basis, the proposed development is estimated to generate approximately 176 vehicle trips on a weekday. Compared to the existing homes the project will generate approximately 9 additional trips during the weekday morning peak hour, 10 additional trips during the weekday evening peak hour and 144 trips over the course of a day. The resulting trip increase is nominal and will result in an additional vehicular trip every 6 to 7 minutes during the peak hours.
- □ *Adequate Roadway Capacity*. The proposed site driveway intersection will operate well below capacity at LOS C during peak hours. Incremental traffic increases at the study intersections due to the proposed development generally result in inconsequential changes in intersection operations compared to No-Build conditions. Therefore, no additional roadway improvements are warranted to accommodate the project.

In summary, trip generation for the development is projected to be modest. MDM finds that incremental traffic associated with the proposed development is not expected to materially impact operating conditions at the study intersections. The available sight lines at the Site Driveway with Lexington Street exceed the recommended sight line requirements from AASHTO. Implementation of recommended improvements as outlined under *Conclusions and Recommendations* will satisfy all applicable design and safety criteria.

PROJECT DESCRIPTION

The existing Site consists of approximately 1.15± acres of land located at 15 & 21 Lexington Street. 15 Lexington Street includes a duplex house, and a separate apartment building, for a total of three units on the property. 21 Lexington includes a single-family home. Access/egress is provided by two driveways along Lexington Street.

Under the proposed site programming, the existing buildings will be removed and a 2 story, 24unit multi-family apartment development will be constructed with 51± parking spaces (22 garage spaces and 29 surface parking spaces). The garage will also provide an area for covered bicycle parking. The proposed access/egress along Lexington Street will be consolidated to a single driveway directly opposite Milton Avenue. The preliminary site plan prepared by Everett M. Brooks Co. is shown in **Figure 2**. Traffic Impact Assessment





EXISTING TRAFFIC & SAFETY CHARACTERISTICS

An overview of existing roadway conditions, traffic volumes, and sight lines is provided below.

Lexington Street

Lexington Street is classified by the Massachusetts Department of Transportation (MassDOT) as an Urban Principal Arterial under local (City) jurisdiction. Lexington Street is generally a north-south roadway in the project area which connects Route 30 to the south and Route 20 to the north in Waltham. Adjacent to the Site, Lexington Street provides two-way traffic flow, has a width of approximately 28 feet with one travel lane in each direction and no shoulders. There are sidewalks on both sides of Lexington Street within the study area. The regulatory (posted) speed limit along Lexington Street is 25 mph in both travel directions within the study area. Land use along Lexington Street within the project area includes a mix of land uses including but not limited to single family homes, apartments, restaurants, retail and office buildings.

River Street

River Street is classified by the Massachusetts Department of Transportation (MassDOT) as a Rural Minor Collector under local (City) jurisdiction. River Street is generally an east-west roadway in the project area which connects Lexington Street to the west and Waltham Street to the east. River Street provides two-way traffic flow, has a width of approximately 30 feet with one travel lane in each direction and no shoulders. There are sidewalks on both sides of River Street within the study area. The regulatory (posted) speed limit along River Street is 25 mph in both travel directions within the study area. Land use along River Street within the project area includes a mix of land uses including but not limited to single family homes, apartments, restaurants, retail and office buildings.

Rumford Avenue

Rumford Avenue is classified by the Massachusetts Department of Transportation (MassDOT) as a Local Road under local (City) jurisdiction. Rumford Avenue is generally an east-west roadway in the project area which connects Forest Grove Road to the west and Lexington Street to the east. Rumford Avenue provides two-way traffic flow, has a width of approximately 30 feet with one travel lane in each direction and no shoulders. There are sidewalks on both sides of Rumford Avenue within the study area. The regulatory (posted) speed limit along Rumford Avenue is 25 mph in both travel directions within the study area. Land use along River Street within the project area includes a mix of land uses including but not limited to single family homes, apartments, restaurants, retail and office buildings.

Traffic Volumes

Traffic volume data were collected at the primary study area intersection during the weekday morning (7:00 AM - 9:00 AM) and weekday evening (4:00 PM – 6:00 PM), periods to coincide with peak traffic activity of the proposed use and the adjacent streets Review of MassDOT permanent count station data indicates that November is an average traffic month, therefore, no adjustment for seasonal fluctuations was required. The weekday morning and weekday evening peak hour traffic volumes for the study intersection are shown in **Figure 3**. Traffic count data and MassDOT permanent count station data are provided in the **Attachments**.

Daily traffic volumes along Lexington Street, south of the Waltham town line were collected in November 2018 and are summarized in **Table 1**. Detail traffic count data is included in the **Attachments**.

TABLE 1 BASELINE TRAFFIC VOLUME SUMMARY LEXINGTON STREET AT WALTHAM TOWN LINE

					Peak Hour
	Daily	Percent	Peak Hour	Peak Flow	Directional
Time Period	Volume (vpd) ¹	Daily Traffic ²	Volume (vph) ³	Direction ⁴	Volume (vph) ⁴
Weekday Morning Peak Hour	15,010	7%	1,065	51% SB	546
Weekday Evening Peak Hour	15,010	8%	1,205	52% NB	629

¹Two-way daily traffic expressed in vehicles per day without seasonal adjustment.

²The percent of daily traffic that occurs during the peak hour.

³Two-way peak-hour volume expressed in vehicles per hour.

⁴NB = Northbound, SB = Southbound

As summarized in **Table 1**, the weekday daily traffic volume on Lexington Street is approximately 15,010 vehicles per day (vpd) on a weekday. Peak hour traffic flow on Lexington Street ranges from approximately 1,065 to 1,205 vehicles per hour (vph) representing approximately 7 to 8 percent of daily traffic flow.

Measured Travel Speeds

Vehicle speeds were obtained for Lexington Street near the Site using a radar recorder. These measured travel speeds provide a basis for determining sight line requirements at the proposed site driveway. **Table 2** presents a summary of the travel speed data collected for Lexington Street in the site vicinity. Collected speed data are provided in the **Attachments**.



2018 Baseline Conditions Weekday Peak Hour Traffic Volumes

TABLE 2SPEED STUDY RESULTS – LEXINGTON STREET

Travel	Regulatory	Travel Speed							
Direction	Speed Limit ¹	Mean ²	85 th Percentile ³						
Northbound Southbound	25 25	25 25	29 29						

¹Regulatory Speed limit in miles per hour (mph).

²Arithmetic mean

³The speed at or below which 85 percent of the vehicles are traveling

As summarized in **Table 2**, the mean (average) travel speed on Lexington Street was observed to be 25 mph in the northbound and 25 mph in the southbound direction. The 85th percentile travel speeds were observed to be 29 mph in the northbound direction and 29 mph in the southbound direction.

Sight Line Evaluation

An evaluation of sight lines was conducted to ensure that minimum recommended sight lines are available at the proposed Site Driveway intersection with Lexington Street. The evaluation documents sight lines under proposed conditions for vehicles as they relate to these roadways with comparison to recommended guidelines.

The American Association of State Highway and Transportation Officials' (AASHTO) standards¹ reference two types of sight distance which are relevant at the intersection: stopping sight distance (SSD) and intersection sight distance (ISD). Sight lines for critical vehicle movements at the proposed Site Driveway intersection along Lexington Street was compared to minimum SSD and ISD recommendations for the regulatory and observed travel speeds in the area.

¹ A policy on Geometric Design of Highways and Streets, American Association of State Highway and Transportation Officials (AASHTO), 2018.



Stopping Sight Distance

Sight distance is the length of roadway visible to the motorist to a fixed object. The minimum sight distance available on a roadway should be sufficiently long enough to enable a below-average operator, traveling at or near the design speed limit, to stop safely before reaching a stationary object in its path, in this case, a vehicle exiting onto Lexington Street. The SSD criteria are defined by AASHTO based on design and operating speeds, anticipated driver behavior and vehicle performance, as well as physical roadway conditions. SSD includes the length of roadway traveled during the perception and reaction time of a driver to an object, and the distance traveled during brake application on wet level pavement. Adjustment factors are applied to account for roadway grades when applicable.

SSD was estimated in the field using AASHTO standards for driver's eye (3.5 feet) and object height equivalent to the taillight height of a passenger car (2.0 feet) for the Lexington Street approaches to the proposed Site Driveway. **Table 3** presents a summary of the available SSD as they relate to Lexington Street and AASHTO's recommended SSD based on regulatory and observed speeds.

TABLE 3 STOPPING SIGHT DISTANCE SUMMARY LEXINGTON STREET APPROACHES TO PROPOSED SITE DRIVEWAY

		AASHTO R	Recommended ¹
Approach/	Available SSD	Regulatory	85 th Percentile
Travel Direction		Speed Limit ²	Travel Speed ³
Northbound	>500 Feet	155 Feet	190 Feet
Southbound	>500 Feet	155 Feet	190 Feet

¹Recommended sight distance based on AASHTO, A Policy on Geometric Design of Highways and Streets. Based on driver height of eye of 3.5 feet to object height of 2.0 feet.

²Regulatory speed limits: 25 mph NB & SB

^{385th} Percentile travel speed: 29 mph NB & SB

As summarized in **Table 3**, analysis results indicate that the available sight lines will exceed AASHTO's recommended SSD criteria along Lexington Street for the regulatory and observed 85th percentile travel speeds. Stopping sight distance calculations are provided in the **Attachments**.

Intersection Sight Distance

Clear sight lines provide sufficient sight distance for a stopped driver on a minor-road approach to depart from the intersection and enter or cross the major road. As stated under AASHTO's Intersection Sight Distance (ISD) considerations, "...If the available sight distance for an entering ...vehicle is at least equal to the appropriate stopping sight distance for the major road, then drivers have sufficient sight distance to avoid collisions...To enhance traffic operations, intersection sight distances that exceed stopping sight distances are desirable along the major road." AASHTO's ISD criteria are defined into several "cases". In this case, the proposed Site Driveway approach will be under "STOP" control. The ISD in question relates to the ability to turn either right or left onto Lexington Street.

Available ISD was estimated in the field using AASHTO standards for driver's eye (3.5 feet), object height (3.5 feet) and decision point (8 to 14.5 feet from the edge of the travel lane) for the northbound and southbound travel directions on Lexington Street. **Table 4** presents a summary of the available ISD for the departures from the proposed Site Driveway and AASHTO's recommended ISD assuming clearing and maintenance of vegetation within the sight line triangles.

TABLE 4

		AASHTO Minimum ¹	AASHTO Ideal ¹
Approach/		85 th Percentile	Regulatory
Travel Direction	Available ISD	Travel Speed ³	Speed Limit ²
Looking North	>500 Feet	190 Feet	240 Feet
Looking South	>500 Feet	190 Feet	280 Feet

INTERSECTION SIGHT DISTANCE SUMMARY PROPOSED SITE DRIVEWAY DEPARTURES TO LEXINGTON STREET

¹Recommended sight distance based on AASHTO, A Policy on Geometric Design of Highways and Streets. Based on driver height of eye of 3.5 feet to object height of 2.0 feet. Minimum value as noted represents SSD per AASHTO guidance.

²Regulatory speed limits: 25 mph NB & SB

³85th Percentile travel speed: 29 mph NB & SB

The results of the ISD analysis presented in **Table 4** indicate that the available sight lines looking north and south from the proposed Site Driveway onto Lexington Street will exceed the sight line requirements from AASHTO for the regulatory and 85th percentile travel speeds. MDM recommends that any new plantings (shrubs, bushes) or physical landscape features to be located within the sight lines should also be maintained at a height of 2 feet or less above the adjacent roadway grade to ensure unobstructed lines of sight.

Intersection Crash History

In order to identify crash trends and safety characteristics for study area intersections, crash data were obtained from MassDOT for the City of Newton for the five-year period 2014 through 2018 (the most recent data currently available from MassDOT). Crash data for the study intersection is summarized in **Table 5** with detailed data provided in the **Attachments**.

Crash rates were calculated for the study area intersections as reported in **Table 5**. This rate quantifies the number of crashes per million entering vehicles. MassDOT has determined the official District 6 (which includes the City of Newton) crash rate to be 0.71 for signalized intersections and 0.52 for unsignalized intersections. These rates represent MassDOT's "average" crash experience for District 6 communities and serves as a basis for comparing reported crash rates for the study intersections. Where calculated crash rates notably exceed the district average, some form of safety countermeasures may be warranted. A review of Highway Safety Improvement Project (HSIP) locations was also conducted.

TABLE 5 INTERSECTION CRASH SUMMARY 2014 THROUGH 20181

	Lexington Street at	Lexington Street at
Data Category	Rumford Avenue/River Street	Milton Avenue
Traffic Control	Signalized	Unsignalized
Crash Rate ²	0.37	0.04
MHD Dist. 6 Avg ³	0.71	0.52
Year:		
2014	1	0
2015	5	0
2016	2	0
2017	2	1
<u>2018</u>	<u>3</u>	<u>0</u>
Total	13	1
Туре:		
Angle	4	0
Rear-End	5	1
Head-On	0	0
Sideswipe	2	0
Single Vehicle	2	0
Severity:		
P. Damage Only	9	1
Personal Injury	4	0
Fatality	0	0
Conditions:		
Dry	11	1
Wet	1	0
Snow	1	0
Time:		
7:00 to 9:00 AM	1	0
4:00 to 6:00 PM	1	0
Rest of Day	11	1

¹Source: MassDOT Crash Database

²Crashes per million entering vehicles (MEV) ³District 6 Average Crash Rate

As summarized in **Table 5**:

- □ *Lexington Street at Rumford Avenue/River Street.* A total of thirteen (13) crashes were reported at the intersection during the five-year study period resulting crash rate of 0.37. The crashes involved six (6) angle/sideswipe type collisions (46%), five (5) rear-end collisions (38%), and two (2) single vehicle type collision. The majority (69%) resulted in property damage only type collisions with 85% of the collisions occurring under dry roadway conditions. The majority (785) of the crashes occurring outside the peak commuter periods. There was one injury type pedestrian related crash and no reported fatalities.
- Lexington Street at Milton Avenue. One (1) crash was reported at the intersection during the five-year study period resulting crash rate of 0.04. The reported crash was a rearend collision which resulted in property damage only and occurred under dry roadway conditions. The crash occurred outside the peak commuter periods and no pedestrians were involved.
- □ *Lexington Street at 15-21 Lexington Street.* There were no reported crashes reported along Lexington Street near the existing site driveways during the study period.

In summary, the study intersections experienced crash rates well below the District 6 average and none of the intersections as high crash locations (HSIP eligible) by MassDOT. No immediate safety countermeasures are warranted based on the crash history at the study intersections.

Public Transportation Facilities

The Massachusetts Bay Transit Authority (MBTA) operates four (4) bus Routes with service within ¹/₄ mile of the Site as follows:

- Route 170 provides service between Central Square in Waltham and Central Square in Waltham with a stop in the immediate Site vicinity at the corner of Lexington Street and Whitlowe Road. Service is generally provided Monday through Friday 5:11 am to 1:19 am, Saturdays between 5:40 am and 1:27 am and Sundays between 6:45 am and 1:23 am.
- Routes 505/553/554 provide service between Central Square in Waltham and Waverly Square in downtown Boston with a stop in the immediate Site vicinity at the corner of Lexington Street and Whitlowe Road. Service is generally provided Monday through Friday 5:55 am to 10:29 pm and Saturdays between 6:25 am and 7:46 pm.

To remain conservative no credit (trip reduction) was taken for the use of nearby public transportation. Specific route and schedule information is provided in the **Attachments**.



FUTURE CONDITIONS

Evaluation of the proposed development impacts requires the establishment of a future baseline analysis condition. This section estimates future roadway and traffic conditions with and without the proposed development. To be consistent with industry standard guidelines for projects not requiring State review, a five-year planning horizon was selected.

To determine the impact of Site-generated traffic volumes on the roadway network under future conditions, baseline traffic volumes in the study area were projected to a future year condition. Traffic volumes on the roadway network at that time, in the absence of the development (that is, the No-Build condition), would include existing traffic, new traffic due to general background traffic growth, and traffic related to specific development by others that is currently under review at the local and/or state level. Consideration of these factors resulted in the development of No-Build traffic volumes. Anticipated Site-generated traffic volumes were then superimposed upon these No-Build traffic-flow networks to develop future Build conditions.

The following sections provide an overview of future No-Build traffic volumes and projected Build traffic volumes.

Background Traffic Growth

Nearby permanent count station data published by MassDOT indicates a 0.1 percent per year growth rate. For purposes of this evaluation, a 0.5-percent compounded annual growth rate was used (2.5 percent increase over a 5-year horizon). This growth rate is higher than historic rates and is also expected to account for any small fluctuation in hourly traffic as may occur from time to time in the study area and traffic associated with other potential small developments or vacancies in the area. MassDOT permanent count station data and background growth calculations are provided in the **Attachments**.

Additionally, based on a review of the MEPA database and discussions with the City of Newton Planning Staff there is one (1) site-specific area development project under construction at the time of the traffic counts that may increase traffic at the study intersections compared to baseline conditions:

□ **143** *Rumford Avenue*: This development is a three story 107,397 s.f. self-storage facility and a separate 5,520 s.f. medical office building that was under construction at the time of the traffic counts on Rumford Avenue in Newton, MA. Traffic associated with this development were estimated based on industry standard rates for mini warehousing (ITE LUC 151) and for Medical-Dental Office Building (ITE LUC 720) and distributed on the traffic volume network based on existing traffic patterns. The site-specific trip tracings are provided in the **Attachments**.

2023 No-Build Traffic Volume Networks

To account for future traffic growth in the study area, the 0.5 percent annual growth rate was applied to existing traffic volumes over a five-year period as well as traffic associated with the one site-specific development in the area. Future 2023 No-Build traffic volumes are displayed in **Figure 4**.

<u>Site-Generated Traffic – ITE Basis</u>

The trip generation estimates for the proposed development are provided for the weekday morning and weekday evening peak hours, which correspond to the critical analysis periods for the proposed use and adjacent street traffic flow. New traffic generated by the project was estimated using trip rates published in ITE's *Trip Generation*² for the Land Use Code (LUC) 220–Multifamily Housing – Low Rise. **Table 6** presents the trip-generation estimates for the proposed development based on ITE methodology.

TABLE 6TRIP-GENERATION SUMMARY

	Site	Trips	
Period/Direction	Existing ¹	Proposed ²	Δ
Weekday Morning Peak Hour:			
Entering	0	3	3
Exiting	<u>2</u>	<u>8</u>	<u>6</u>
Total	2	11	9
Weekday Evening Peak Hour:			
Entering	2	8	6
Exiting	<u>1</u>	<u>5</u>	<u>4</u>
Total	3	13	10
Weekday Daily (24 hours)	32	176	144

¹Based on ITE LUC 210 (Single Family Home) applied to 1 unit and 220 (Multifamily Housing – Low Rise) applied to 3 units. ²Based on ITE LUC 220 (Multifamily Housing – Low Rise) applied to 24 dwelling units

²Trip Generation, 10th Edition; Institute of Transportation Engineers; Washington, DC; 2017.



2023 No-Build Conditions Weekday Peak Hour Traffic Volumes As summarized in **Table 6**, the proposed development is estimated to generate approximately 11 vehicle trips (3 entering and 8 exiting) during the weekday morning peak hour and 13 vehicle trips (8 entering and 5 exiting) during the weekday evening peak hour. On a daily basis, the proposed development is estimated to generate approximately 176 vehicle trips on a weekday. Compared to the existing homes the project will generate approximately 9 additional trips during the weekday morning peak hour, 10 additional trips during the weekday evening peak hour and 144 trips over the course of a day. The resulting trip increase is nominal and will result in an additional vehicular trip every 6 to 7 minutes during the peak hours. Trip generation calculations are provided in the **Attachments**.

Trip Distribution

The directional distribution of development-generated trips on the roadway network is a function of a number of variables including area population centers and the efficiency of these roadways leading to the Site. Existing traffic patterns served as the primary basis for determining the trip distribution pattern for the project. Detailed calculations are provided in the **Attachments**.

Development-related trips for the proposed apartment development are assigned to the roadway network using the trip-generation estimates shown for the proposed Site in **Table 6** and the distribution patterns presented in **Figure 5**. To remain conservative no credit (trip reduction) was taken for existing residential units at the Site. Development-related trips at each intersection approach for the weekday morning and weekday evening peak hours are quantified in **Figure 6**.

Build Traffic Volumes

Build condition traffic volumes are derived by adding incremental traffic increases for the proposed apartments to the No-Build traffic volume networks. The resulting 2023 Build condition traffic-volume networks for the weekday morning and weekday evening peak hours are displayed in **Figure 7**.





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Site Generated Trips Weekday Peak Hour Traffic Volumes



2023 Build Conditions Weekday Peak Hour Traffic Volumes

CAPACITY ANALYSIS

Capacity analysis of intersections is developed using the Synchro® computer software, which implements the methods of the 2010 Highway Capacity Manual (HCM). The resulting analysis presents a level-of-service (LOS) designation for individual intersection movements. The LOS is a letter designation that provides a qualitative measure of operating conditions based on several factors including roadway geometry, speeds, ambient traffic volumes, traffic controls, and driver characteristics. Since the LOS of a traffic facility is a function of the traffic flows placed upon it, such a facility may operate at a wide range of LOS, depending on the time of day, day of week, or period of year. A range of six levels of service are defined on the basis of average delay, ranging from LOS A (the least delay) to LOS F (delays greater than 50 seconds for unsignalized movements and delays greater than 80 seconds for signalized movements). The specific control delays and associated LOS designations are presented in the **Attachments**.

Level-of-Service (LOS) analyses were conducted for the Baseline, No-Build, and Build conditions for the study intersections. The results of the intersection capacity are summarized below in **Table 7** and **Table 8**. Detailed analysis results are presented in the **Attachments**.

TABLE 7 INTERSECTION CAPACITY ANALYSIS RESULTS WEEKDAY MORNING PEAK HOUR

		2	2018 Baseliı	ne	2	023 No-Bui	ld	2023 Build															
Peak Hour	Approach	v/c ¹	Delay ²	LOS ³	v/c	Delay	LOS	v/c	Delay	LOS													
Lexington Street at Rumford	Eastbound Westbound	0.43 0.44	25 19	C B	0.47 0.47	26 20	C B	0.47 0.47	26 20	C B													
Avenue/River Street	Northbound <u>Southbound</u>	0.49 <u>0.90</u>	8 <u>26</u>	А <u>С</u>	0.53 <u>0.94</u>	9 <u>33</u>	А <u>С</u>	0.53 <u>0.95</u>	9 <u>34</u>	А <u>С</u>													
	Overall	0.90	20	С	0.94	23	С	0.95	24	C													
Lexington Street	EB Exit	n/a	n/a	n/a	n/a	n/a	n/a	0.01	12	В													
at Site Driveway	WB Exit	WB Exit	WB Exit	WB Exit	WB Exit	WB Exit	WB Exit	WB Exit	WB Exit	WB Exit	WB Exit	WB Exit	WB Exit	0.03	03 17	C	0.03	0.03 17	17	С	0.04	20	С
Milton Avenue	Northbound	n/a	n/a	n/a	n/a	n/a	n/a	0.00	<5	А													
	Southbound	0.00	<5	А	0.00	<5	А	0.00	<5	А													

¹Volume-to-capacity ratio

² Average control delay per vehicle (in seconds)

³Level of service

TABLE 8 INTERSECTION CAPACITY ANALYSIS RESULTS WEEKDAY EVENING PEAK HOUR

			2018 Baselin	ne	2	023 No-Bui	ld	2023 Build			
Peak Hour	Approach	v/c ¹	Delay ²	LOS ³	v/c	Delay	LOS	v/c	Delay	LOS	
Lexington Street	Eastbound	0.50	23	С	0.59	27	С	0.60	27	С	
at Rumford	Westbound	0.62	26	С	0.69	29	С	0.69	29	С	
Avenue/River	Northbound	0.46	7	А	0.49	8	А	0.49	8	А	
Street	Southbound	0.69	<u>13</u>	<u>B</u>	0.73	<u>14</u>	<u>B</u>	0.73	<u>14</u>	<u>B</u>	
	Overall	0.69	14	В	0.73	16	В	0.73	16	В	
Lexington Street	EB Exit	n/a	n/a	n/a	n/a	n/a	n/a	0.02	20	С	
at Site Driveway	WB Exit	0.02	18	С	0.02	19	С	0.03	22	С	
Milton Avenue	Northbound	n/a	n/a	n/a	n/a	n/a	n/a	0.00	<5	А	
	Southbound	und 0.01 <5 A				<5	А	0.01	<5	А	

¹Volume-to-capacity ratio

² Average control delay per vehicle (in seconds)

³Level of service

As shown in Table 7 and Table 8:

- □ *Lexington Street at Rumford Avenue/River Street.* Under No-Build conditions the signalized intersection will operate at an overall LOS C or better during peak hours. The proposed development does not result in any significant change in operations at the signalized intersection compared to No-Build conditions.
- □ *Lexington Street at Site Driveway/ Milton Avenue.* Under Build conditions the site driveway approach to the Lexington Street will operate with at LOS C or better during peak hours.

In summary, the proposed development does not result in any significant change in operations at the study intersections compared to No-Build conditions.

RECOMMENDATIONS AND CONCLUSIONS

Trip generation for the development is projected to be nominal during commuter peak hours. MDM finds that incremental traffic associated with the proposed development is not expected to materially impact operating conditions at the study intersections. The study intersection exhibits a below-average crash rate based on historic crash data; safety countermeasures are therefore not warranted. Likewise, the available sight lines at the proposed Site Driveway intersection with Lexington Street exceed the recommended sight line requirements from AASHTO.

MDM recommends the following improvements to enhance safety and capacity:

- □ *Signage and Markings.* A STOP sign (R1-1) and STOP line pavement markings are recommended on the proposed Site Driveway approach to Lexington Street. The sign and pavement markings shall be compliant with the Manual on Uniform Traffic Control Devices (MUTCD).
- □ *On-Site Circulation & Driveway Design.* The proposed site driveway intersection Lexington Street should be designed to accommodate the City's largest fire apparatus (ladder truck), refuse trucks, and single unit delivery vehicles. Likewise, the final design of the circulation aisles and parking layout should provide adequate maneuvering area for the largest potential responding vehicle (ladder truck).
- *Pedestrian Accommodation.* A sidewalk connection between the building and parking will be provided. Additionally, a sidewalk connection to the existing sidewalk system along Lexington Street will be provided.
- □ *Bicycle Accommodations.* The development has incorporated weather protected bicycle storage within the multi-family building for residents.
- □ *Sight Line Maintenance.* Any new plantings (shrubs, bushes) or physical landscape features to be located within the project driveway sight lines should also be maintained at a height of 2 feet or less above the adjacent roadway grade to ensure unobstructed lines of sight.

In summary, trip generation for the development is projected to be modest. MDM finds that incremental traffic associated with the proposed development is not expected to materially impact operating conditions at the study intersections. The available sight lines at the Site Driveway intersection with Lexington Street exceed the recommended sight line requirements from AASHTO. Implementation of recommended improvements will satisfy all applicable design and safety criteria.

Attachments

- □ Traffic Volume Data
- □ Speed Data
- Seasonal/Yearly Growth Data
- \Box Crash Data
- □ Public Transportation Facilities
- □ Sight Line Analysis
- □ Background Growth
- □ Trip Generation Calculations
- □ Trip Distribution Calculations
- □ Capacity Analysis

.

□ Traffic Volume Data

Lexington Street At Waltham Town Line North of Site Drive Newton, MA

MDM Transportation Consultants, Inc. 28 Lord Road, Suite 280 Marlborough, MA 01752 508-303-0370 Da www.mdmtrans.com

Date Start: Tuesday, November 06, 2018 Site Code: 888 Station ID:

Date Start: Tuesday, November 06, 2018

Start	Tuesday,	South	bound	Hour	Totals		North	bound		Combined Totals		
Time	Tue	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	
12:00		9	96			18	100					
12:15		5	101			10	105					
12:30		5	115			17	102					
12:45		5	122	24	434	7	124	52	431	76	865	
01:00		2	93			7	121					
01:15		7	108			7	110	일하는 것 같은 것 같				
01:30		5	100			5	102					
01:45		800 - H-I-I	107	15	408	6	127	25	460	40	868	
02:00		4	114			2	114					
02:15			115			3	135					
02:30		3	118			2	120					
02:45		3	98	11	445	2	126	9	495	20	940	
03:00		2	134			0	129					
03:15		4	128			3	128				Yan Banada da	
03:30		2	123			6	141					
03:45		2	111	10	496	2	124	11	522	21	1018	
04:00	na ta tu cintesetti teo na ti a	4	92			6	142		or the second second second			
04:15		6	107		01403040430	4	143				202969696	
04:30		8	88			7	130					
04:45		16	84	34	371	8	126	25	541	59	912	
05:00		20	92			17	124					
05:15		33	97			25	138					
05:30		40	82			31	140			na ma kana ƙwalana ka k	a landa a la san	
05:45	sus sere as h	45	80	138	351	56	158	129	560	267	911	
06:00		53	85		or and a financial	50	165					
06:15		86	57		erene pereze	64	148		en de la company de la comp			
06:30	ène tana ammenina an co	113	65			68	137			a ta san na <u>a mu</u> neo s		
06:45		113	60	365	267	93	117	275	567	640	834	
07:00	to average the strength of the second	118	63		VERILIA PARA PARA 15	74	103	ana ana an				
07:15		109	[2]		alle Sator	107	101					
07:30	an a	135	[2]			101	86				ودويو تهر دو در در در در در د	
07:45		100	71	462	278	108	73	390	363	852	641	
00:00	orde verste het de stande v	100	61			130	83					
08:15		99	50		ong ng ng sa	122	68		. Calegia de Brateleo			
08:30		94	59	204	000	143	00		200	000	500	
08:45		101	50	394	220	140	69	535	280	929	000	
09:00		99 70	34		usu kashulana baha	134	IC C		e pas te te te e company.			
09:15		76	45		asse viteste i	126	53		a seconde de la compañía de la comp Compañía de la compañía			
09:30		12	34			127	04 50	CONTRACTOR	ംംംം	047	070	
09,45		01	30	328	148	132	52	213	230	047	370	
10.00		90 76	29			119	44		una pone ar por	eren waaren ara		
10.13	editects Debit Ser	02	30		NGNA NGCO	114	42 AE	european ann an t-	a ka ngangangangangangangangangangangan ka		buvus astronom	
10.30		30	32 04		447	91 07	40	400	150	770	076	
10:40	abade serb a RCEO	104	21	3/U	11/	0/ 100	2/	409	100	(19	213	
11.00		100	20			001	24 25	SECTION OF THE SECTION OF T	o falles Nils (s délation)			
11.10		0E	46		rant Milièdh.	94 114	20	e nava nej Crevensi	na ana ang Kabupatèn (0.0000000000000000000000000000000000000		
11.30		00 70	10	200	04		29 1 A	407		707	170	
Total	ang katalan UTA (193	25/1	3622	390	01	2796	14	40/	32	131 5207	<u></u>	
I Utal		41 20/	59.9%			2100	62.8%			39.0%	61.0%	
Combined		41.270	JU.070			51.270	02.070			59.070	01.078	
Total		616	63			74	85			1364	8	

Page 1

Lexington Street At Waltham Town Line North of Site Drive Newton, MA

MDM Transportation Consultants, Inc. 28 Lord Road, Suite 280 Marlborough, MA 01752 508-303-0370 Da www.mdmtrans.com

Date Start: Tuesday, November 06, 2018 Site Code: 888 Station ID:

Date Start: Tuesday, November 06, 2018

Start	Wednesda	Southbound		Hour	Totals		North	bound		Combined Totals			
Time	Wed	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon		
12:00		7	95	v		17	105	Ŭ		v			
12:15		14	119			17	102						
12:30		7	105			11	115						
12:45		3	88	31	407	10	98	55	420	86	827		
01:00		10	96			9	115		······				
01:15		3	130			6	122						
01:30		4	115			8	109						
01:45		4	120	21	461	200 7 /	102	30	448	51	909		
02:00		6	109			3	102						
02:15		4	99			0	103						
02:30		7	131			5	101						
02:45		5	114	22	453	5	117	13	423	35	876		
03:00		3	127			0	115						
03:15		2	134			2	113						
03:30		7	137			6	128						
03:45		3	108	15	506	3	131	11	487	26	993		
04:00		4	147			5	144						
04:15		13	141			15	123						
04:30		7	109			7	131						
04:45		17	126	41	523	9	153	36	551	77	1074		
05:00		22	145			11	154						
05:15		28	153			22	154						
05:30		45	145			30	160						
05:45		60	132	155	575	54	161	117	629	272	1204		
06:00		65	118			63	166						
06:15		88	126			72	152						
06:30		120	110			80	138						
06:45		119	102	392	456	76	123	291	579	683	1035		
07:00		144	121			89	126						
07:15		95	99			75	118						
07:30		127	72			91	95						
07:45		144	77	510	369	107	100	362	439	872	808		
08:00		153	87			117	83						
08:15		144	87			126	82						
08:30		105	68	n fan Karana an fan mar de 1. fer		150	68						
08:45		144	61	546	303	124	64	517	297	1063	600		
09:00		115	59			132	75						
09:15		103	73			152	51		n de puestes				
09:30		106	38			117	71						
09:45		97	53	421	223	104	49	505	246	926	469		
10:00		98	52			121	68						
10:15		91	54			103	70		CERSENCS				
10:30		102	38			74	42	an a sharan <u>aray a</u> a d		ana yana <u>men</u> ana			
10:45	and Hereinis	99	22	390	166	78	28	376	208	766	374		
11:00	nuorana engalarinaria arun area des	86	25			101	42						
11:15		92	25		pansesse	102	26		6661666666				
11:30		100	17			109	23						
11:45	<u> 1998/06/1997</u>	94	17	372	84	109	17	421	108	793	192		
Iotal		2916	4526			2734	4835			5650	9361		
Percent		39.2%	60.8%			36.1%	63.9%			37.0%	62.4%		
		74	42			75	69			150	11		

Marlborough, MA

N/S: Lexington Street E/W: River Street/Rumford Avenue Newton, MA

	Groups Printed- Lights - Mediums - Articulated Trucks																				
		Lexi	naton	Street		[R	ver Str	eet			Lexi	ington	Street							
		F	rom No	orth			F	rom Ea	ast		From South					From West					
Start Time	Right	Thru	Left	Peds	App. Tetal	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
07:00 AM	0	62	17	0	79	3	6	7	0	16	2	45	12	0	59	9	1	1	0	11	165
07:15 AM	1	93	28	0	122	14	7	5	0	26	2	62	19	0	83	8	5	3	0	16	247
07:30 AM	9	104	45	0	158	7	2	13	0	22	7	67	15	0	89	9	8	5	0	22	291
07:45 AM	7	106	45	0	158	15	12	12	0	39	9	67	15	0	91	11	10	11	0	32	320
Total	17	365	135	0	517	39	27	37	0	103	20	241	61	0	322	37	24	20	0	81	1023
08:00 AM	6	123	48	0	177	17	9	13	0	39	10	63	16	0	89	13	11	13	0	37	342
08:15 AM	6	111	50	0	167	36	16	19	0	71	16	84	13	0	113	13	18	7	0	38	389
08:30 AM	6	147	48	0	201	33	9	17	0	59	8	77	14	0	99	13	15	4	0	32	391
08:45 AM	2	140	57	0	199	37	15	10	0	62	17	91	24	0	132	8	15	6	0	29	422
Total	20	521	203	0	744	123	49	59	0	231	51	315	67	0	433	47	59	30	0	136	1544
04:00 PM	4	114	39	0	157	23	11	8	0	42	6	105	16	0	127	31	21	9	0	61	387
04:15 PM	11	111	51	0	173	50	6	18	0	74	10	100	8	0	118	15	8	5	0	28	393
04:30 PM	4	89	32	0	125	37	10	18	0	65	14	101	8	0	123	20	10	5	0	35	348
04:45 PM	6	102	38	0	146	34	13	16	0	63	11	107	12	0	130	21	12	11	0	44	383
Total	25	416	160	0	601	144	40	60	0	244	41	413	44	0	498	87	51	30	0	168	1511
05:00 PM	6	102	38	0	146	33	17	19	0	69	6	115	6	0	127	30	16	6	0	52	394
05:15 PM	6	101	48	0	155	29	16	21	0	66	15	111	9	0	135	25	17	8	0	50	406
05:30 PM	5	85	41	0	131	36	11	18	0	65	9	114	7	0	130	23	15	8	0	46	372
05:45 PM	4	104	55	0	163	21	13	18	0	52	12	109	7	0	128	22	16	6	0	44	387
Total	21	392	182	0	595	119	57	76	0	252	42	449	29	0	520	100	64	28	0	192	1559
Grand Total	83	1694	680	0	2457	425	173	232	0	830	154	1418	201	0	1773	271	198	108	0	577	5637
Apprch %	3.4	68.9	27.7	0		51.2	20.8	28	0		8.7	80	11.3	0		47	34.3	18.7	0		
Total %	1.5	30.1	12.1	0	43.6	7.5	3.1	4.1	0	14.7	2.7	25.2	3.6	0	31.5	4.8	3.5	1.9	0	10.2	
Lights	73	1627										1363									
% Lights	88	96	95.1	0	95.5	93.9	91.3	96.6	0	94.1	97.4	96.1	96	0	96.2	91.5	94.4	81.5	0	90.6	95
Mediums	9	55	28	0	92	24	15	8	0	47	4	52	7	0	63	20	9	11	0	40	242
% Mediums														-		-					
Articulated Trucks	1	12	5	0	18	2	0	0	0	2	0	3	1	0	4	3	2	9	0	14	38
% Articulated Trucks	1.2	0.7	0.7	0	0.7	0.5	0	0	0	0.2	0	0.2	0.5	0	0.2	1.1	1	8.3	0	2.4	0.7

Marlborough, MA

	<u> </u>	Lexi	ngton	Street			Ri	ver St	treet			Lexi	ngton	Street			Rum	ford A	venue		
		F	rom No	orth			F	rom E	ast			Fr	om So	outh		From West					
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	int. Total
Peak Hour A	\nalysi	is Fror	n 07:0	0 AM t	o 11:45	AM -	Peak '	1 of 1													
Peak Hour f	or Enti	re Inte	ersectio	on Beg	ins at 0	8:00 A	M														
08:00 AM	6	123	48	0	177	17	9	13	0	39	10	63	16	0	89	13	11	13	0	37	342
08:15 AM	6	111	50	0	167	36	16	19	0	71	16	84	13	0	113	13	18	7	0	38	389
08:30 AM	6	147	48	0	201	33	9	17	0	59	8	77	14	0	99	13	15	4	0	32	391
08:45 AM	2	140	57	0	199	37	15	10	0	62	17	91	24	0	132	8	15	6	0	29	422
Total Volume	20	521	203	0	744	123	49	59	0	231	51	315	67	0	433	47	59	30	0	136	1544
% App. Total	2.7	70	27.3	0		53.2	21.2	25.5	0		11.8	72.7	15.5	0		34.6	43.4	22.1	0		
PHF	.833	.886	.890	.000	.925	.831	.766	.776	.000	.813	.750	.865	.698	.000	.820	.904	.819	.577	.000	.895	.915
Lights	18	494	186	0	698	116	47	54	0	217	48	297	66	0	411	43	53	20	0	116	1442
% Lights	90.0	94.8	91.6	0	93.8	94.3	95.9	91.5	0	93.9	94.1	94.3	98.5	0	94.9	91.5	89.8	66.7	0	85.3	93.4
Mediums	2	19	12	0	33	7	2	5	0	14	3	18	1	0	22	4	4	7	0	15	84
% Mediums	10.0	3.6	5.9	0	4.4	5.7	4.1	8.5	0	6.1	5.9	5.7	1.5	0	5.1	8.5	6.8	23.3	0	11.0	5.4
Articulated Trucks					1																
% Articulated Trucks	0	1.5	2.5	0	1.7	0	0	0	0	0	0	0	0	0	0	0	3.4	10.0	0	3.7	1.2



MDM Transportation Consultants, INC.

28 Lord Road, Suite 280 Marlborough, MA

		Lexi Fi	ngton rom N	Street orth		River Street From East						Lexi Fr	ngton rom So	Street outh							
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Tolal	int. Total
Peak Hour A	Peak Hour Analysis From 12:00 PM to 05:45 PM - Peak 1 of 1																				
Peak Hour for Entire Intersection Begins at 05:00 PM																					
05:00 PM	6	102	38	0	146	33	17	19	0	69	6	115	6	0	127	30	16	6	0	52	394
05:15 PM	6	101	48	0	155	29	16	21	0	66	15	111	9	0	135	25	17	8	0	50	406
05:30 PM	5	85	41	0	131	36	11	18	0	65	9	114	7	0	130	23	15	8	0	46	372
05:45 PM	4	104	55	0	163	21	13	18	0	52	12	109	7	0	128	22	16	6	0	44	387
Total Volume	21	392	182	0	595	119	57	76	0	252	42	449	29	0	520	100	64	28	0	192	1559
% App. Total	3.5	65.9	30.6	0		47.2	22.6	30.2	0		8.1	86.3	5.6	0		52.1	33.3	14.6	0		
PHF	.875	.942	.827	.000	.913	.826	.838	.905	.000	.913	.700	.976	.806	.000	.963	.833	.941	.875	.000	.923	.960
Lights	20	382	177	0	579	115	51	75	0	241	41	438	26	0	505	94	62	28	0	184	1509
% Lights	95.2	97.4	97.3	0	97.3	96.6	89.5	98.7	0	95.6	97.6	97.6	89.7	0	97.1	94.0	96.9	100	0	95.8	96.8
Mediums	1	9	5	0	15	4	6	1	0	11	1	11	2	0	14	6	2	0	0	8	48
% Mediums							10.5	1.3	0	4.4	2.4	2.4	6.9	0	2.7	6.0	3.1	0	0	4.2	3.1
Articulated Trucks			-							_						_	_	_	_	_	
% Articulated Trucks	0	0.3	0	0	0.2	0	0	0	0	0	0	0	3.4	0	0.2	0	0	0	0	0	0.1



Marlborough, MA

N/S: Lexington Street E/W: River Street/Rumford Avenue Newton, MA

	Groups Printed- Bicycles or													on Road - Pedestrians										
		Lexin	igton	Street			Ri	ver St	reet			Lexir	ngton	Street										
		Fre	om No	orth			Fi	rom E	ast			Fr	om So	outh										
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	int. Total			
07:00 AM	0	0	0	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1			
07:15 AM	0	0	0	0	0	0	0	0	1	1	0	0	0	2	2	0	0	0	2	2	5			
07:30 AM	1	0	0	0	1	0	0	0	0	0	0	0	0	3	3	0	0	0	0	0	4			
07:45 AM	0	1	0	0	1	0	0	0	3	3	0	0	0	2	2	0	0	0	3	3	9			
Total	1	1	0	1	3	0	0	0	4	4	0	0	0	7	7	0	0	0	5	5	19			
08:00 AM	0	0	0	1	1	0	0	0	3	3	0	0	0	2	2	0	0	0	2	2	8			
08:15 AM	0	0	0	3	3	0	0	0	0	0	0	0	0	1	1	0	0	0	1	1	5			
08:45 AM	0	0	0	1	1	0	0	0	1	1	0	0	0	0	0	0	0	0	3	3	5			
Total	0	0	0	5	5	0	0	0	4	4	0	0	0	3	3	0	0	0	6	6	18			
		•	~	~	0.1	•	~	~	•	a	•	~	~	40	40	•	~	~		ا م	~			
04:00 PM	0	0	0	0	0	0	0	0	2	2	0	0	0	18	18	0	0	0	1	1	21			
04:15 PM	0	0	0	0	0	0	0	0	1	1	0	0	0	U	0	0	0	0	1	1	2			
04:30 PM	0	0	0	1	1	0	0	0	1	1	0	0	0	0	0	0	0	0	2	2	4			
04:45 PIVI	0	0			- 0		0		0	0	0	0		1	10	0	<u> </u>	0	1	1	<u></u>			
Iotal	0	0	0	1	1	0	U	0	4	4	U	U	0	19	19	0	U	U	5	5	29			
OSILE DM	0	0	0	0		0	0	0	0	0	0	0	^		4	0	0	0	0	0	4			
05.10 PM	0	0	ő	0		0	ő	ŏ	0	Ň	ő	ő	č	- -	4	0	ň	Ň	ŏ	Ň	2			
05.30 FM	0	õ	0	1	1	0	0		0	0	0	0	0		2	ŏ	ŏ	0	ŏ	Ň	2			
Total	0			- 1			<u> </u>			- 0	- 0	- 0		7	7	0			- 0	- 0	2			
rotar	U	0	U	1	• •	U	U	0	0	01	0	0	0	'	1	U	U	0	0	0	0			
Grand Total	1	1	Λ	8	10	0	Ω	٥	12	12	0	0	٥	36	36	Ο	0	٥	16	16	74			
Apprch %	10	10	ň	80		ň	ň	ň	100	12	ň	ň	ñ	100	50	ň	ő	ñ	100	10	77			
Total %	14	14	ň	10.8	13.5	ň	ň	ñ	16.2	16.2	ñ	ň	ñ	48.6	48.6	ň	õ	ň	21.6	21.6				
Bicycles on Post	1.7	1.7	<u> </u>		10.0		v		.0.2	10.2	0		5	10.0		v	~	J	~ 1.0					
% Biogries on Road	100	100	0	0	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.7			
Pedestrians	0	0	0	8		Ō	ō	0	12	12	ō	Ō	Ō	36	36	0	Ō	Ő	16	16	72			
% Pedestrians	ō	ō	ō	100	80	õ	õ	õ	100	100	õ	ō	õ	100	100	ō	Ō	ō	100	100	97.3			
	-	-	-			-	-	-			-	-	-		1	-	-	2						

Marlborough, MA

		Lexi	ngton	Street		River Street						Lexi	ngton	Street							
		Fr	om N	orth		From East						Fr	om So	buth			1				
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour A	Peak Hour Analysis From 07:00 AM to 11:45 AM - Peak 1 of 1																				
Peak Hour for Entire Intersection Begins at 07:15 AM																					
07:15 AM	0	0	0	0	0	0	0	0	1	1	0	0	0	2	2	0	0	0	2	2	5
07:30 AM	1	0	0	0	1	0	0	0	0	0	0	0	· 0	3	3	0	0	0	0	0	4
07:45 AM	0	1	0	0	1	0	0	0	3	3	0	0	0	2	2	0	0	0	3	3	9
08:00 AM	0	0	0	1	1	0	0	0	3	3	0	0	0	2	2	0	0	0	2	2	8
Total Volume	1	1	0	1	3	0	0	0	7	7	0	0	0	9	9	0	0	0	7	7	26
% App. Total	33.3	33.3	0	33.3		0	0	0	100		0	0	0	100		0	0	0	100		
PHF	.250	.250	.000	.250	.750	.000	.000	.000	.583	.583	.000	.000	.000	.750	.750	.000	.000	.000	.583	.583	.722
Bicycles on Road																					1
% Bicycles on Road	100	100	0	0	66.7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7.7
Pedestrians	0	0	0	1	1	0	0	0	7	7	0	0	0	9	9	0	0	0	7	7	24
% Pedestrians	0	0	0	100	33.3	0	0	0	100	100	0	0	0	100	100	0	0	0	100	100	92.3



Marlborough, MA

		Lexi	ngton	Street		River Street						Lexi	ngton	Street							
		Fr	om N	orth		From East						Fr	om Sc	buth							
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
Peak Hour Analysis From 12:00 PM to 05:45 PM - Peak 1 of 1																					
Peak Hour f	2eak Hour for Entire Intersection Begins at 04:00 PM																				
04:00 PM	0	0	0	0	0	0	0	0	2	2	0	0	0	18	18	0	0	0	1	1	21
04:15 PM	0	0	0	0	0	0	0	0	1	1	0	0	0	0	0	0	0	0	1	1	2
04:30 PM	0	0	0	1	1	0	0	0	1	1	0	0	0	0	0	0	0	0	2	2	4
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	0	0	0	1	1	2
Total Volume	0	0	0	1	1	0	0	0	4	4	0	0	0	19	19	0	0	0	5	5	29
% App. Total	0	0	0	100		0	0	0	100		0	0	0	100		0	0	0	100		
PHF	.000	.000	.000	.250	.250	.000	.000	.000	.500	.500	.000	.000	.000	.264	.264	.000	.000	.000	.625	.625	.345
Bicycles on Road																					
% Bicycles on Road	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Pedestrians	0	0	0	1	1	0	0	0	4	4	0	0	0	19	19	0	0	0	5	5	29
% Pedestrians	0	0	0	100	100	0	0	0	100	100	0	0	0	100	100	0	0	0	100	100	100



□ Speed Data
North of Site Di Newton, MA	rive						508-3(www.mdn	03-0370 ntrans.corr	_					۵	ate Start: C Site (S	06-Nov-18 Code: 888 tation ID:
														C	ate Start. C	6-Nov-18
Southbound														Ċ		
Start	-	16	21	26	31	36	41	46	51	56	61	66	71	76		85th
Time	15	20	25	30	35	40	45	50	55	60	65	70	75	666	Total	Percent
11/06/18	-	2	7	12	2	0	0	0	0	0	0	0	0	0	24	29
01:00	0	0	4	80	e	0	0	0	0	0	0	0	0	0	15	ы Э
02:00	0	0	7	7	2	0	0	0	0	0	0	0	0	0	-	30
03:00	0	0	0	7			0		0	0	0	0	0	0	9	37
04:00	. -	9	7	11	9	ო	0	0	0	0	0	0	0	0	34	33
02:00	. -	7	28	79	27	~-	0	0	0	0	0	0	0	0	138	31
00:90	-	24	147	164	27	-	0		0	0	0	0	0	0	365	29
02:00	38	86	205	124	6	0	0	0	0	0	0	0	0	0	462	27
08:00	7	34	140	164	45	4	0	0	0	0	0	0	0	0	394	29
00:60	0	24	122	141	36	ъ	0	0	0	0	0	0	0	0	328	29
10:00	0	15	148	158	48	~~	0	0	0	0	0	0	0	0	370	29
11:00	0	22	124	206	34	4	0	0	0	0	0	0	0	0	390	29
12 PM	7	43	236	129	23		0	0	0	0	0	0	0	0	434	28
13:00	2	37 2	206	140	22	~	0	0	0	0	0	0	0	0	408	28
14:00	2	64	214	145	18	7	0	0	0	0	0	0	0	0	445	28
15:00	2	55	282	141	16	0	0	0	0	0	0	0	0	0	496	27
16:00	8	41	187	123	თ	ო	0	0	0	0	0	0	0	0	371	28
17:00	ო	67	192	86	0		0	0	0	0	0	0	0	0	351	27
18:00	~	42	127	93	4	0	0	0	0	0	0	0	0	0	267	28
19:00	~-	30	140	92	14		0	0	0	0	0	0	0	0	278	28
20:00	~-	1 3	108	88	16	0	0	0	0	0	0	0	0	0	226	28
21:00		თ	57	64	15	0	0	0	0	0	0	0	0	0	148	29
22:00	0	8	40	51	15	ო	0	0	0	0	0	0	0	0	117	30
23:00	0	4	35	32	ω	2	0	0	0	0	0	0	0	0	8	29
Statistics	1) MPH Pace (Speed :	21-30 M	Hd											
		85th Perc	centile :	28 M	Hd											
		95th Per	centile :	31 N	Hd											
	Number of	Vehicles > 25	: MPH :	0	705											
	Percent of	Vehicles > 25	: MPH :	43.	6%											
	Ă	san Speed(Av	erage) :	25 N	IPH											

Page 1

MDM Transportation Consultants, Inc. 28 Lord Road, Suite 280 Mariborough, MA 01752

Lexington Street At Waltham Town Line

Page 2	-Nov-18 ode: 888 ttion ID:	-Nov-18 85th	Percent	3 X X	32	35	58 58 58	28	29 31	59	28 20	67 56	29	29 28 28	27	58 78	29 29	29	29 32		
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		71	75	00	00	00	00	0	0 0	00	00	00	0	0 0	00	00	00	0	00		
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		6 6	7	00	⊃ 	<i>←</i> ς	28	87	13 01	15	<u>8</u>	31	34	62 70	86	55 41	19	9	5	10 MPH P 85th 95th of Vehicles of Vehicles Mean Spee	Mean Spee 85th 95th of Vehicles of Vehicles
	eet own Line Drive	- ų	0	00	00	00	°₽	49	0 0	0	- n	,	ოი	15 e	~	o -	- 0	0	00	Number Percent	Number Percent
	Lexington Stre At Waltham Tr North of Site E Newton, MA	Southbound Start	11/07/18	01:00	03:00	04:00	00:00	00:00	00:60	10:00	11:00 12 PM	13:00	14:00	16:00	17:00	18:00 19:00	20:00	21:00	22:00 23:00	Statistics	Stats

Page 2

Mbund Image 1 5 3 36 41 46 51 56 61 66 71 76 Time 1 2 2 31 36 41 46 51 56 61 66 71 76 <th< th=""><th>rth of Site Dr wton, MA</th><th>ive</th><th></th><th></th><th></th><th></th><th></th><th>508-3 www.mdi</th><th>mtrans.com</th><th> _</th><th></th><th></th><th></th><th></th><th>Δ</th><th>ate Start: (Site (S</th><th>)6-Nov-18 Code: 888 tation ID:</th></th<>	rth of Site Dr wton, MA	ive						508-3 www.mdi	mtrans.com	_					Δ	ate Start: (Site (S)6-Nov-18 Code: 888 tation ID:
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22:00 3 11 54 73 15 2 0 0 0 0 0 158 29 23:00 1 5 28 41 15 1 1 0 0 0 0 0 0 0 92 31 23:00 1 5 28 41 15 1 1 0 0 0 0 0 0 92 31 10 MPH Pace Speed: 21-30 MPH 85th Percentile: 29 MPH 92 31 10 MPH Pace Speed: 21-30 MPH 3301 935th Percentile: 3204 11 55 MPH 3301 95th Percentile: 3201 941.% Number of Vehicles > 25 MPH 3301 941.% 955. 941.% 941.% Mercent of Vehicles > 25 MPH 25 MPH 2301 941.% 956. 941.% Mercent of Vehicles > 25 MPH 25 MPH 250. 941.% 941.% 941.% Mercent of Vehicles > 25 MPH 25. 941.% 941.% 941.% 941	21:00	τŋ (×o :	98	c01	4	N	0	0	0	0	0	0	0	0	230	29
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tistics 10 MPH Pace Speed: 21-30 MPH 85th Percentile: 29 MPH 95th Percentile: 32 MPH Number of Vehicles > 25 MPH: 3301 Percent of Vehicles > 25 MPH: 44.1% Mean Shore/Averane): 25 MPH: 26 MPH	23:00	-	5	28	41	15	-	-	0	0	0	0	0	0	0	92	31
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B5th Percentile 29 MPH 95th Percentile 32 MPH Number of Vehicles > 25 MPH 33.01 Percent of Vehicles > 25 MPH 44.1% Mean Shoed(Averane) 25 MPH	atietine	4	ADH Dace	. poord	21.20 M												
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Percent of Vehicles > 25 MPH : 44.1% Mean Sneed(Average) : 25 MPH		Number of	Vehicles > 25	: HdM	. ຕັ	301											
Mean Sneed(Averane) · 25 MPH		Percent of	Vehicles > 25	: HAM	44	.1%											
		AA	an Sneed/Ave	. (anara	25 M	На											

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Lexington Street At Waltham Town Line

MDM Transportation Consultants, Inc. 28 Lord Road, Suite 280 Marlborough, MA 01752

Page 4	06-Nov-18 Code: 888 Station ID:	06-Nov-18	85th Percent	33		8 8 8	31	- R	စ္က စ္က	31 30	888	30 30	29 28	2 9 F	27 29	29	29	32			
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			30 30	6 5	9	10	63 138	144	217 208	165 175	162	184	173 150	110	145	123	121	52	21-30 25 25 25	33 26	•
			21 25	16 8	c	o و	23 67	95	144	84 125	150	134	175 206	297	200	96 1	77 55	18	Pace Speed : h Percentile : h Percentile : > 25 MPH : > 25 MPH : od(Average) :	d(Average) : h Percentile : h Percentile : > 25 MPH :	: > 25 MPH :
			16 20	დო	00	0	6 8	00	4 7 0 7 0	37 40	27 35	56	58 112	165	49	37	4 5 6	00	10 MPH F 85th 95th of Vehicles of Vehicles Mean Spee	Mean Spee 85tl 95tl of Vehicles	of Vehicles
et wofine			1 15	0 +	4 4	- 0	с v О		4 (8 0	17	5 12 8	45 45	84 %	2 2 2	ოი	m ≁.	•	Number Percent	Number	Percent
Lexington Stree	North of Site D Newton, MA	Northbound	Start Time	11/07/18 01:00	02:00 03:00	04:00	05:00 06:00	00:20	00:00	10:00 11:00	12 PM	14:00	15:00 16:00	17:00	19:00	20:00	21:00 22:00	23:00	Statistics	Stats	

Page 4

Seasonal/Yearly Growth Data

	STATION 691	- QUINCY - F	TE.I-93 - NO	RTH OF RTE.	28								
60	JAN 173,000	FEB 175.000	MAR 177.697	APR 194.334	MAY 196.834	199.477	JUL 196.208	AUG 194 125	SEP 190 AR5	OCT 186 291	NOV 176 509	DEC 174 000	YEAR
:	-2%	%0	4%	-1%	-1%	%0	-1%	-1%	1%	1%	3%	4%	0.5%
11	166,541 -2%	175,019 6%	190,696 0%	192,155 0%	193,034 1%	197,594	193,303	191,197	193,140	188,694	187,378	187,895	188,054
12	164,007	185,226	190,193	192,337	194,846	195,145	-1%	370 196,457	-1% 190,548	-2% 185,609	0% 186,469	-3% 181.669	-0.1% 187.827
ţ	9% 9%	-1% 187 813	-5%	-3%	-1%	0%	%0	1%	%0	2%	-1%	-3%	-0.1%
2	%8- 8%	% <i>L</i> -	3%	3%	130,139	134,012	192,130	191,401 0%	191,411	190,128	185,233 0%	176,163 5%	187,554 0.2%
- 14	165,955 3%	170,581	187,003	193,263	194,348	198,176	193,591	197,456	193,827	192,895	185,667	185,147	188,159
15	171,029	159,322	-0%	174,319	-0% 178,128	172,060	-3% 187,071	3% 202.569	3% 198.773	197.111	4% 192.381	4% 192.770	-1.4% 183.069
ţ	4%	%6	% 8	%2	%2	3%	5%	1%	1%	1%	1%	1%	3.8%
I/ Seasonal Adjustment Factor	171,001	169,054	139,012	0.99	202,004	181,236 0.99	205,446 0.97	207,586 0.95	200,920 0.97	199,524 0.98	198,080 1.01	194,984	196,853
(to average month)												Growth	0.47%
Ş	STATION 703	- ABINGTON	- RTE.123 -	AT THE BROG	CKTON C.L.								
80 80	JAN 12,251	13,199	MAK 13,301	APK 13,860	MAY 13,231	JUN 13,817	JUL 13.354	AUG 13.212	SEP 14.037	0CT 13.712	13 161	DEC 13.327	YEAR 13.372
ç	%0 %0	%0	2%	1%	5%	1%	%0	1%	-1%	%0	2%	-1%	0.8%
2	-5%	4%	-1%	-4%	-3%	13,300	-3%	13,338 -2%	13,928 -1%	13,/33	13,414 0%	13,225 1%	13,472 -2 0%
ŧ	11,629	12,651	13,451	13,518 19/	13,476	13,655	12,907	13,088	13,778	13,495	13,434	13,377	13,205
12	12,181	13,151	13,410	-1%	13,452	-1% 13,479	-6% 12.127	13.103	-2%	13.679	0% 13.452	-2% 13.136	-0.3% 13 166
5	1%	-6% %9-	4%	2%	%0	-1%	%4	%0	%0	%0	-2%	%0	-0.3%
2	140'71 4%	3%	3%	13,251	13,420 -1%	13,3/2	12,964 -2%	13,064 -1%	13,462 -1%	13,726 -3%	13,217	13,081 2%	13,121 -0 5%
14	11,894	12,651	13,252	13,385	13,345	13,524	12,759	12,893	13,376	13,379	12,882	13,315	13,055
15	11.974	-5% 11.975	40 12 649	-2% 13 151	0% 13.378	-1%	17 879	12 941	-1%	-1%	0%0 10 868	-2% 10 085	-1.3%
: :	1%	3%	3%	-1%	-2%	1%	-1%	%0	-1%	-1%	-1%	%0 %0	0.1%
16 Seasonal Adiustment Easter	12,035	12,304	13,075	13,076	13,171	13,574	12,742	12,986	13,061	13,140	12,743	12,940	12,904
(to average month)	60.1	5	<u>8</u> .	16'0	0.90	0.31	20.1	10.1	0.97	/A.U	DO. L	Growth	-0.50%
	STATION 416	- 1-95/ ROU	TE 128 SOUT	H OF 1-90									
Υ,	JAN	FEB	MAR	APR	MAY	NUL	JUL	AUG	SEP	OCT	NON	DEC	YEAR
12	130,033 1%	133,659 -6%	138,451 0%	142,034 3%	158,583 -7%	148,787 1%	138,599 10%	144,999	141,340 6%	146,271 5%	140,898 2%2	128,666 1%	141,027
13	131,812	125,662	138,122	145,780	147,000	149,925	151,813	149,393	150,507	153,009	143,498	130,116	143,053
14	-5% 125.340	127 134	3% 142 024	3% 150 125	3% 151 576	3% 153 Q16	-5% 144 679	0% 149 503	151 538	-1%	-1% 111 876	6% 137 pre	0.6%
	6%9	1%	2%	%0	1%	1%	1%	1%	%0	1%	2%	%0	1.2%
16	139,436 3%	130,154	148,054	149,295 20/	153,957	156,496 20/	147,414 500	151,081	152,186	154,663	146,935	137,768	147,287
17	134,884	130,641	129,731	-3%	153,434	156,333	147,884	-1% 149,113	154,281	1% 155,618	149,129	147,141	-0.8%
Seasonal Adjustment Factor (to average month)	1.09	1.12	1.04	0.99	0.94	0.94	0.99	0.97	0.96	0.95	1.00	1.06 Growth	0.60%
	STATION 625	- WEYMOU	TH - RTE.3 - I	NORTH OF R	TE.18								
YR 80	NAL	FEB 173 063	MAR 424 867	APR	MAY 105 200	NUL	JUL	AUG	SEP	OCT	NON	DEC	YEAR
80 80	120,200	3%	124,8U/ 6%	134,354 -1%	852'CEL	143,114 -1%	143,685 -1%	144,937 -2%	140,079 -3%	137,288	138,708 -1%	136,428 -7%	135,235 -0.6%
10	125,304	127,637	132,301	133,124	135,880	141,633	141,706	142,327	135,767	133,473	137,526	127,100	134,482
12	118.936	-1%	-1% 129.712	-0% 116.911	U% 136 235	140.277	-1% 139.048	0%0 142 140	-1% 132 674	-2% 128 923	-3% 129 593	-1%	-1.5% 130 AAG
ş	4%	%2-	-4%	13%	%0	-1%	1%	%0	1%	4%	-1%	-1%	0.3%
5	123,/83 -8%	100'011 %C	724,813	755,151 %0	136,712 -1%	1/6'92L	140,057	141,851	133,978 2%	134,144	128,712	124,607	131,306
14	113.701	118439	127037	131150	135,571	139,606	147,748	147,593	136,789	132,227	143,498	130,116	133,623
16	120,926	121003	128951	132915	1% 138,071	142,406	-2% 140,685	-2% 142,991	0% 135,630	134,163	-5% 129,976	0% 128.837	-0.2% 133,046
54	3% %E	3%	»0 %0	1%	%0	%0	-1%	-1%	%I	-1%	1%	%0	0.1%
Seasonal Adjustment Factor (to average month)	1.10	1.09	1.04	1.02	0.98	0.94	0.94	0.93	011,461	1.00	0.99	128,//5 1.03 Growth	-0.16%
Average	NAL	FEB	MAR	APR	MAY	NUL	JUL	AUG	SEP	OCT	NON	DEC	
Seasonal Adjustment Factor (to average month)	1.09	1.08	1.02	0.99	0.97	0.96	0.98	0.96	0.97	0.98	1.00	1.03	

ITALICS = ESTIMATED DATA MADT

> Average Yearly Growth Calculated 0.1% Yearly Growth Factor Used 0.5%

> > Page 1 of 1

Crash Data



INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : <u>Newton, M</u>	A			COUNT DA	ATE :	Nov-18
DISTRICT : 6	UNSIGN	IALIZED :] SIGN	ALIZED :	X
		~ IN	TERSECTIO	N DATA ~		
MAJOR STREET :	Lexigton Str	eet				
MINOR STREET(S) :	Rumford Ave	enue/River St	reet			

	I ↑		Lexingto	on Street 3)	1	
INTERSECTION	North	<u></u>		,		
DIAGRAM (Label Approaches)		Rumford Aver (1)	nue		River Street (2)	
			Lexingto	on Street 4)		
			PEAK HOUI		S	
APPROACH :	1	2	3	4	5	Total Peak Hourly
DIRECTION :	EB	WB	SB	NB		Approach Volume
PEAK HOURLY VOLUMES (PM) :	192	252	595	520		1,559
"K" FACTOR :	0.080] INTERS	ECTION ADT APPROACH	" (V) = TOT H VOLUME :	AL DAILY	19,488
TOTAL # OF CRASHES :	13	# OF YEARS :	5	AVER/ CRASHES	AGE # OF S PER YEAR(A):	2.60
CRASH RATE CALCU	LATION :	0.37	RATE =	<u>(A*1</u> (V	,000,000) * 365)	
Comments : MassDOT	District 6 Avg	: Signalized =	0.71; Unsign	alized = 0.52	2	

Project Title & Date: 888 - Newton



INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : Newton, N	IA			COUNT DA	ATE:	Nov-18
DISTRICT :6	UNSIGN	ALIZED :	X] SIGN/	ALIZED :	
		~ IN	TERSECTIO	N DATA ~		
MAJOR STREET :	Lexigton Str	eet				
MINOR STREET(S) :	Milton Avenu	ue				
INTERSECTION DIAGRAM (Label Approaches)	 North		Lexingto (Lexingto	on Street 3) on Street 4)	River Street (2)	
APPROACH :	1	2	3	4	5	Total Peak Hourly
DIRECTION :	EB	WB	SB	NB		Approach Volume
PEAK HOURLY VOLUMES (PM) :		9	546	514		1,069
"K" FACTOR :	0.080		ECTION ADT APPROACH	(V) = TOT, I VOLUME :	AL DAILY	13,363
TOTAL # OF CRASHES :	1	# OF YEARS :	5	AVERA CRASHES	GE # OF PER YEAR ():	0.20
CRASH RATE CALCU	LATION :	0.04	RATE =	<u>(A*1,</u> (V	000,000) * 365)	
Comments : MassDOT	District 6 Avg	: Signalized =	0.71; Unsign	alized = 0.52		

Project Title & Date: 888 - Newton

	Men Mender Tree		P1 Pedestrian		P3-Pedalcyciist (bicycle, haceda uniceda padal carl											
	Distance from Maximum Institute															
	Delayse from Never Ed															
	Datance from Neerest Milementer	100000														
	Cistance from Prantial Roadway Interbedian															
	At Roschery Entertaction		LEXINGTON ST / RIVER ST		LEXINGTON ST / MIYER SIL LEXINGTON ST / RUMFORD AVE	LEXINGTON STREET /	LEXINGTON STREET / RIVER STREET	RIVER ST /LEXINGTON ST	LEXINGTON STREET / RUMFORD AVENUE	LEXINGTON STREET / RUMFORD AVENUE	LEXINGTON ST / MILTON	RUMFORD AVE / LEXINGTON ST	LEXINGTON STREET / RUMFORD AVENUE	LEXINGTON STREET / RUNFORD AVEN IF	LEXINGTON STREET /	LEXINGTON STREET /
	Ventret Condition		Zear	,	Abudy Abudy	1	, is a second	Jear/Glear	a a a a a a a a a a a a a a a a a a a	jej,		, A	Jan	Sear	t de	, re
	now Light		antant			ediothi C	5		aviont	eviore 0	ark - lighted	Z	and at the second s	avient C	tion to the total to the total tota	- Alectric
	Rowd Burdace	and a constant of the second se	8	<u>6</u>	Wet D	C	 }	0	<u>ه</u>	 	60	8	8	 &		 8
	erios Confgueitor.	1: Light truck(van, mini-van,	anel, pickup, eport utility) with civ four tites	1: Light truck(van, mini-ran, ny four lines / V2 Pessenger ny four lines / V2 Pessenger ar / V3 Light truck(van, mmi- art, penel, pickup, spot Lidiky) art, penel, pickup, spot Lidiky)	1. Passencer car	11: Single-unit truck (2-axie, 6- re) / V2 Passenorer car	1: Pessenger car / V2.Light uck(var, mini-van, panel, ickup, sport utilih) with only Arr tires	11. Pessenger car / 2. Passenger car.	(1: Passenger car / 1: Passenger car / 2: Unknown heavy Iruck	1. ((Light Indektvan, mini-van, ickup, sport utiliky)) / V2. (Light uck(van, mini-van, pickup, bort utiliky)	1: (Light trock(van, mini-van, ckup, spot uitiny) / 3: Passerget cn1 / /	11:(Light truck(ven, mint-ven, icidup, sport utility)) / V2:(Light uck(ven, mint-ven, pickup, boot utility)	1 (Light truck(van, mini-van, sckup, sport utility)) / 2 (Passender carl)		11.(Light truck(van, mini-van, ickup, sport utility) / 2.(Passenoer cart)	11 (Passenger car) / 2 (Passenger car)
	Most Harmhil Evens	<u>v</u>	V1: Collision with pedestrian	V1: Cotation with moder V1: Cotation with moder verhicke in using / V2: Collision of with moder verhicle in (adfic / o with moder with moder version in range	V1: Collision with cyclist (bloyde, tricycle, unicycle, pedal car)	V1: Cotision with motor whicle in traffic / V2: Collision V with motor vehicle in traffic ti	V1: Collision with motor which in traffic / V2: Collision p with motor which in fraffic h	V1: Collision with motor vehicle in traffic / V2: Collision V with motor vehicle in traffic	V1: Collision with motor V1: Collision with motor vehicle in traffic / V2: Collision With motor vehicle in traffic on	V1:(Coltsion with molor V vehicle in traffic) / V2.(Coltsion with molor to vehicle in traffic) s	V1: (Collision with motor whide in traffic) / V2 (Collision with motor vehicle in traffic) / V3 (Collision with motor vehicle in traffic) /	V1:(Cottation with motor vehicle in traffic) / V2:(Cottation with motor vehicle in traffic)	V1:(Colision with motor vehicle in (raffic) / V2:(Colision with motor prothicle in (raffic)	V1: (Collision with pedestrian)	V1:(Colitison with motor vehicle in traffic) / V2:(Colision with motor vehicle in traffic)	V1:(Colision with motor vehicle in traffic) / V2:(Colision with motor vehicle in traffic)
	Vehicle Trave Directions		V1 Northbound	V1:Southbound / V2:Southbound / V3:Southbound /	V1Eastbound	V1:Westbound / V2.Westbound /	V1: Narthbound / V2: Southbound /	V1:Northbound / V2 Eastbound	VI: Southbound / V2 Westbound	V1:Southbound / V2.Netthbound	V1: Southbound / V2: Southbound / V2: Southbound /	V1.Westbound / V2.Westbound /	V1:Wettbound / V2.Wettbound /	V1: Southbound	V1:Southbound / V2:Westbound	V1:Westbound / V2:Westbound
- 2018	Vencie Action Prior to Creek		V1: Tuming right	V1: Slowing or stopped in Itellic / V2: Slowing or stopped Itellic / V2: Slowing or stopped at teatro: / V3: Traveiling straight	V1: Tuming right	V1: Slowing at strapped in traffic / V2: Travelling straight shead	VI: Traveling straight ahead / V2: Turning left	V1: Traveling straight shead / V2: Tuming left	V1: Stowing or stopped in traffic / V2:Turming left	V1: Traveling straight sheed / V2: Traveling straight sheed	V1: Stowing or stopped in V1: Stowing or stopped in in teffic / V3: Traveling straight sheed	V1: Slowing or stopped in traffic / V2: Slowing or stopped in traffic	V1: Slowing or stopped in traffic / V2: Slowing or stopped in traffic	VI: Travelino straicht eheed	V1: Traveling straight ahead / V2: Turning left	V1: Slowing or slopped in traffic / V2: Slowing or slopped in traffic
the years 2014	d Marrier of Collection	_	Single vehicle crash	Stear-and	Ancie	Rear-end	Anole	Angle	Sideswipe, opposits direction	Sideewipe, opposite direction	Rear-end	Rear-end	Rear + nd	Sincle vehicle crash	Angle	Rear end
ewton for	of Norteth Tota Strijuntee Inju	-	۹ ۲		-	o	0	0	o		°	0	0	101		0
sort for N	Number Vehicles		niurv 1		- I viule	ternege 2	amage 2	lamage 2	lemage 2	tarmage	emage 3	tarmage	tamage 2	niury 1	tamage 2	tarmage
rash Rep	me Cash See	1	I Non-fatal I	Non-fitel in	Non-fatal k	Property d only (none injured)	Property d only (none inlures)	Property d only (none Inlured)	Property d only (none inives)	Property d orty (none iniured)	Property di anty (name 3 PM inivred)	Property d anty (mane M initred)	Property d only (none M inlured)	Non-fatal it	Property d anhy (none iniured)	Property d only (none inkured)
ssDOT C	Dette Cresh 71		<u>uo-2014 8 01 PN</u>		10-2015 6.22 AM	P-2015 7:33 AM	**2015 5.39 AM	+2015 6 29 AM	1-2016 4.40 PM	X-2016 9.16 AM	0.2017	VI-2017 10 02 A	d-2012 12 05 P	V-2018 3.17 PM	0-2018 9.05 AM	
Ma	hame Cresh		28-AU	<u> </u>	23-Au	11-Fei	14-NG		20-Ma	28-AB	6.48	29.1		20.4	21-40	11-25
TOORS	Chyrtonn		NEWTON	NEWTON	NEWTON	NEWTON	NEWTON	NEWTON	NEWTON	NEWTON	NEWTON	NEWTON	NEWTON	79598 NEWTON	28466 NEWTON	45599 NEWTON
ma.	Cresh Number	014	3949680 2018	1100211	1076918	009279	111029	052249	018 1175557	215188	408169	408779	438222	451	462	197

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Public Transportation Facilities

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Route 70 Cedarwood, Market Place Drive, or Central Square, Waltham - University Park Route 70A North Waltham - University Park



70/	70A		Wee	kday				70/7	70A		Satu	rday			
Leave	Inb Leave	ound Arrive	Arrive	Leave	Outb	ound Arrive	Arrive	Leave	Inbc Leave	Arrive	Arrive	Leave	Outbo Leave	Arrive	Arrive
Cedar- wood	North Waitham	Water- town Sq.	University Park	University Park	Water- town Sq.	North Waltham	Cedar- wood	Cedar- wood	North Waltham	Water- town So	University I. Park	University Park	Water- town Sq.	North Waltham	Cedar- wood
5:11A 5:30		5:31A 5:50	5:53A 6:12	4:31A 4:50	4:46A 5:05		5:04A 5:23	5:40A 6:10		5:56A 6:26	6:19A 6:49	5:00A 5:30	5:15A 5:45		5:34A 6:04
5:50 6:10		6:10 6:30	6:33 6:58	5:05 5:20	5:20 5:35		5:38 5:53	6:45 m 7:20		7:01 7:39	7:27 8:05	6:00 m 6:30	6:18 6:48		6:39 7:10
6:30	g 6:10A	6:45 6:49	7:07 7:17	g 5:30 5:40	5:47 5:55	6.04A	6:18	e 8:00	g 7,55A	8:10 8:28	8:37 8:58	g 7:00 7:20	7:21 7:41	7:47A	e 7:52
m 6:45 7:00		7:07 7:23	7:38 7:54	m 5:55 g 6:03	6:13 6:20	6:41	6:39 	8:35	g 9:10	8:54 9:43	9:20 10:13	7:45 g 8:15	8:06 8:36	9.02	8:30
7:18	g 6:55 	7:30 7:41	8:07 8:12	6:08 g 6:21	6:27 6:39	7:04	6:53	m 9:45	g 10:05	10:06 10:40	10:36 11:11	m 8:45 g 9:10	9:06 9:31	9:57	9:31
т 7:27 е 7:44		7:50 7:56	8:21 8:27	6:25 m 6:34	6:44 6:53		7:10 7:19	10:30 e 10:50	••••• ••••	10:55 11:01	11:25 11:29	9:30 g 9:55	9:53 10:16	10;42	10:23
7:47	g 7:29 	8:08 8:10	8;48 8:41	6:45 g 8:53	7:04	7:59	7:30	m 11:15	g 10:50	11:24	11:56	10:05 m 10:15	10:28 10:38	e	10:42
8:00	g 7:55	8:23	8:54 9:06	57:00 7:06	7:16		7:51	6 11:45 	g 11:30	12:06P	12:24 12:38P	10:50	11:13		11:43
8:50	g 8:28	9:05 9:11	9:32	g 7:30	7:58	8:24	8:94	e 12:10P		12:21P	12:49P	g 11:15	11:38	12:10P	12.029
m 9:10	a 9:00	9:31	9:59	g 8:00	8:28	8;54	9.04	e 12:30	a.12·15P	12:41	1:09	m 11:35	11:58		12:28
9:30	a 9:25	9:51 10:00	10:19 10:24	8:20 g 8:30	8:45 8:58	9:22	9:11	m 12:35 e 1:10	•••••	12:58 1:21	1:30 1:49	h 12:00N	12:23P	1:01P	
m 9:50	g 9:55	10:11 10:24	10:39 10:48	m 8:45 g 8:55	9:10 9:20	9:47	9:36	1:20	h 1:10	1:33 1:43	2:03 2:15	12:15P 12:25	12:38 12:48		1:08P e 1:02
10:20 m 10:40		10:41 11:01	11:09 11:29	9:15 m 9:35	9:40 10:00		10:06 10:26	e 1:35 e 1:55	 	1:46 2:06	2:14 2:36	h 12:40 12:50	1:03 1:13	1:41	e 1:27
11:05	g 11:08	11:26 11:42	11:54 12:15P	9:55 g 10:08	10:20 10:33	11:03	10:46	m 2:05	h 1:50	2:13 2:28	2:42 3:00	m 1:00 1:10	1:23 1:33		1:53 e 1:47
m 11:30 11:55		11:51 12:18P	12:23 12:51	m 10:30 10:50	10:55 11:15		11:21 11:41	e 2:35	 h 2:30	2:44 2:54	3:16 3:23	h 1:20 1:35	1:44 1:58	2:22	2:28
m 12:15P		12:38P	1:11P	g 11:10 m 11:16	11:33	12:03P	12:08P	2:40 e 3:10	 	3:03 3:19	3:34 3:51	1:45 h 2:00	2:08	 9:00	0 2:22
12:45	g 12:08P	1:08	1:11	11:40	12:069		12:34	m 3:15	n 3:06	3:30	3:59 4:09	m 2:15 2:25	2:38		3:08 e 3:02
1:40	h 1:25	1:33	2:06	h 12:20P	12:43	1:19P	12:55P	e 3:35 e 3:50	 	3:44	4:10 4:31	n 2:35 2:45	3:08		e 3:22
m 2:00		2:03	2:36	m 12:55	1:02		1:50	3:55		4:18	4:49	3:05	3:28		e 3:42
m 2:46	h 2:30	2:56	3:27	1:25 m 1:45	1:52		2:20	e 4:30	 h 4:20	4:39	5:11	3:25 m 3:35	3:48		e 4:02 4:28
e 3:20 3:17		3:31	3:58	2:08 h 2:20	2:35	3:26	3:02	m 4:40 e 5:00		5:03 5:09	5:33 5:38	3:45 h 4:00	4:08	4:58	e 4:22
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b 12:40 Route 70/	A Indicate	12:47 d by shad	b 1:04	e 12:10A aw 1:04	12:27A 1:19	C	12:35	6:45/ m 7:30	A 7:0 7:4	2A 7	7:25A 8:10	6:00A m 6:45	6:16 7:02	A	6:35A 7:23
Runningt	ime from C	Central Sq	uare and U	niversity Par	k is appro	kimately 2 п	ninutes.	m 9:00	9:1	4 9 4	9:42	m 8:15	6:33 8:59		8:54
a-0 b-1	Fo/from Ce	ntral Squa	are, Wathan	n - Central S	iquare, Ca	mbridge		m 10:00	10:2	0	10:46	m 9:10 9:35	9:28 9:54		9:52 10:18
g - /	AM routing	- serves Trace	Totten Pond	Road & Wy	man Stree	t outbound,	and	m 10:50 11:15	11:1 11:3	0 5	11:36 12:01P	m 9:55 10:20	10:14 10:40	1	10:38 11:04
h - F	M routing	g - serves	Smith Str	et & Trape	lo Road o nd	utbound, a	nd	m 11:40	12:0	ON	12:28	m 10:45 11:05	11:05 11:27	1	11:29 11:51
m - 1 w - 1	lo/From 12 Naits for la	265 Main 8 Ist train to	Shopping C arrive at Ce	enter (Marke entral Souar	et Place Di e Station.	r.), Waltham	·	12:00 m 12:20	N 12:2 12:4	1P 1	12:49P 1:09	m 11:25 11:45	11:47 12:07	P 1	12:11P 12:31
170	In	bound	Wee	kday	Outbo	bnu		m 1:00	1:0	1	1:29 1:49 2:10	m 12:05P	12:27	P 1	12:52P
Leav Central	e / Sa	Arrive Back	Arrive	Leave	Arrh Bac	/e Ar	rive ral So	m 1:40	2:0	0	2:30	m 12:45	1:08		1:33
Waltha	im D	Bay	Station	Station 6:16A	Ba	y Wa	tham 21 A	m 2:20 2:40	2:3	9	3:09 3:29	m 1:20 1:40	1:43 2:03		2:08 2:28
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NO.	service of	1 Weekend	Route	ays- see fai a 70/70A	e intormat	ion on rever	50	m 3:40 4:00	3:5 4:1	9	4:30 4:50	m 2:40 3:00	3:03 3:23		3:28 3:48
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	are	.Lo	cal <u>Bus</u> B	us + Bus	Rapid	Bus + Rapi	d	5:20	5:1 5:4	0	6:13	4:00 4:20 m 4:40	4:25		5:09 5:29
0	harlieCa	rd 85s	1.70	\$1.70	\$2.25	\$2.25		6:00 m 6:20	6:2 6:3	0 9	6:50 7:07	5:00 m 5:20	5:25 5:45		5:49 6:10
Ğ	harlieTic	ket \$	2.00	\$2.00	\$2.75	\$4.75	1	6:40 m 7:00	6:5 7:1	7 7	7:25 7:45	5:40 m 6:00	6:05 6:22		6:30 6:47
C	ash-on-B tudent/Y	oard \$ outh• \$	2.00 0.85	\$4.00 \$0,85	\$2.75 \$1.10	\$4.75 \$1.10		7:20 m 7:35	7:3 7:5	7 2	8:04 8:19	6:20 m 6:40	6:42 7:02		7:06 7:26
S	enior/TA	P•• \$	0.85	\$0.85	\$1.10	\$1.10	~~ ~	7:55 m 8:15	8:1 8:3	1	8:38 8:58	7:00 m 7:20	7:22 7:42		7:46 8:06
(5)	LID PASSES: 1 30.00/mo.); * pat passes.	inkPass (\$84 "Senior/TAP	.50/mo.); Loca LinkPass (\$30,	I Bus (\$55/mo. /mo.); and expr); *Student/Y ess bus, com	outh LinkPass muter rail, and		8:35 9:05	8:5 9:2	1	9:16 9:44	7:40 8:15	8:02		8:57 9:20
FRI	EE FARES: Chi ess CharlieC Requires St	ldren 11 and ard holders ri udent Charlie	l under ride fre ide free and if eCard or Youth	e when accom using a guide, t CharlieCard	panied by an he guide ride tudent Charli	adult; Blind s free. eCards are avai	iable	9:38 10:13 10:45	9:5 10:2	2 7 9	10:48	9:25 10:00	9:08 9:43	1	10:05
	to students are available	through part e through co	ticipating mide	le schools and ters in the Bost	high schools. on metro are	Youth Charliel a. Visit	Cards	11:20	11:3	3 7A	11:53 12:27A	10:35	10:53	1	11:13
••	Requires Se and person	nior/TAP Cha s with disabil	arlieCard, avail lities.	able to Medica:	re cardholder	s, seniors 65+,		b 12:41/	12:4	7	b 1:03	e 12:05A	12:21/	4 e1	2:32A

Holiday information on map side.

 b 12:41A
 12:47
 b 1:03
 e 12:05A
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 e 12:32/ i.aw 1:10

 All buses are accessible to persons with disabilities





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Route 505 Express Bus-Central Square, Waltham - Downtown Boston Route 553 Roberts - Downtown Boston

11. TC 442

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No Route 553 service on Sunday	" No Route 554 service	ner on weekends	6A BAII buses are accessible to persons with disabilities		9 Outer Express–Route 505 fares	4	3 Duter Express Outer Express	6 rate Express + Local Bus + Subway	3 CharlieCard \$5.25 \$5.25	1P Charlie Ticket \$7.00 \$9.00 \$0.75				g Senior/TAP** \$3.50 \$3.50 \$3.50	VAUD PASSES: Outer Express Bus (\$168/mo.), commuter rail zone 1 or higher,	9 FREE FARES: Children 11 and under ride free when accompanied by an adult: Blind	5 Access CharlieCard holders ride free and if using a guide, the guide rides free.	0 * Requires Student ChariteCard or Youth ChariteCard. Student ChariteCards are	A available to students through participating middle schools and high schools. Voith Charlie Contents and the school state of the school state	6 metro area. Visit www.mbta.com/vouthpass for details.	** Requires Senior/TAP CharlieCard, available to Medicare cardholders,	seniors 65+, and persons with disabilities.	NO local fare applies for any portion of Route 505	Route 553 & 554 fares		4A Fare Local Inner Anner Express Inner Express	CUS CAPIESS T CUUCII DUS T CUUMAY	6 CharlieCard \$1.70 \$4.00 \$4.00 \$4.00	4 CharlieTicket \$2.00 \$5.00 \$7.00 \$7.75	9 Cash-on-Board \$2.00 \$5.00 \$7.00 \$7.75	9 Student/Youth* \$0.85 \$2.50 \$2.50			VAUD PASSES: Inner Express Bus (\$128/mo.), Outer Express Bus (\$168/mo.) commuter rail zone 1 or higher on extress and 1A and higher on local	and boat passes.	FREE FARES: Children 11 and under ride free when accompanied by an adult; Blind Access CharleCard holders ride free and if using a quide the order free free	Requires Student CharileCard or Youth CharlieCard. Student CharlieCards are available	to students through participating middle schools and high schools. Youth CharlieCards are available through community partners in the Boston metro area. Visit	7 www.mbta.com/youthpass for details. ** Benuives Centry/PAD CharlieCard anality to Medicare controp 65.	2 and persons with disabilities.	7	12 F Fall 2018 & Winter 2019 Holidays 9/3/18: see Sunday 10/3/18: see Weekday	12 1 122/18, 1225/18, 12/18, 12/18: see Sunday 1/2/19 & 2/18/19: see Saluiday
rday	Arriv	Corn	6:56	7:41	8:20	9:17	10:01	10:46	11.3	12:21	ţ	24			40,4	4:40	5:35	6:20	7:01	7:46		raay	7		Robe	6:54	7:4	8:26	9:12	9:55	10:4	50.00	7.71	1 . .1		2.3	3.15	4	4:4	5:3	6:13	2	÷
Satu	Атіve	Central Sq. Waltham	6:38A	7:23	8:10	8:55	9:40	10:25	11:12	11:58	000.01	104.21	1.5	2:57	3:42	4:27	5:12	5:56	6:40	7:25	0.04	Satu	Outbound	Arrive	Valtham	6:42A	7:28	8:13	00:6	9:45	10:33	81.11	100:21	19-500	1.25	2:19	3:04	3:49	4:33	5:18	6:03	6:48	12)
553		Leave Roberts	6:30A	7:15	8:00	8:45	9:30	10:15	11:00	11:45	10.000	1.15	2.00	2:45	3:30	4:15	5:00	5:45	6:30	7:15	623	202		Leave	Corner	6:30A	7:15	8:00	8:45	9:30	10:15	11:00	C+	12-30P	1.15	2:00	2:45	3:30	4:15	5:00	5:45	6:30	613
		Arrive Roberts		6:41A		7:03	7:26	i	8:39		2. 2. 2.	10:38	3	11:36		12:38P		1	1:34P		2:33		3:37	1	4:42	5.37		6:41		7:35	1	i	1	1	1								-
	Arrive	Waverley Square	6:41A		7:07	1	-	7:46	no stanto tra trans	9:04	10.07	10.01	10-59		11:59	1		1:03P	1	2:03	ļ	3:07	I	4:04		5:09	6:23		7:19	1	1	I		ł	1					E.A.		quare-	101900
Outbound	Arrive	Central Sq. Waltham	6:20A	6:29	6:45	6:51	7:14	7:24	8:18 5 :5	8:48	9. 17 D. KS	10.00	10:45	11:17	11:45	12:16P		12:47P	1:17	1:47	2:17	2:49	3:23	3:52	4:28	4:52 5-18	6:06	6:28	7:04	7:22	7:47	8:10	8:28	9:00	10.23	teologi	c	iy square		Route 5			
	Arrive	Newton Corner	6:04A	6:13	6:28	6:35	6:58	7:07	7:56	8:27	0.00	a.v. 10:01	10:23	10:56	11:23	11:54		12:25P	12:55	1:25	1:55	2:25	2:56	3:25	4:01	4:22	5:33	6:01	6:37	6:56	7:22	7:50	8:11	8:41	21.20	ed areas		la copie			VALUE:		22
кdау	Leave	Downtown Boston	t 5:51A	5:58	t 6:15	6:20	6:43	t 6:50	7:40	8:10 9:40	0.40	0.45	10:10	10:40	11:10	11:40		12:10P	12:40	1:10	1:40	2:10	2:40	3:10	3:45	4:35	5:04	5:35	6:10	6:40	c 7:00	c 7:30	c 7:50	c 8:20	C 3.30	d by shade	MI-MI-	vvaltnam v					
Weel	Arrive	Downtown Boston	7:19A		8:02	8:18	8:32	8:50	9:10	9:42 40:04	10.01	50.1	11:37	12:01	12:37P	And	1:01P	1:36	2:01	2:36	3:02	3:36	4:04	4:41	5:16	5:46 6:26	6:46	7:25	7:38	8:19	8:30	8.6	9:41		-	t indicate	0	al square,	nan		0.0	lale,	
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pupoqu	Lv/Arrive	Central Sq. Waltham	6:36A	2:00	7:14	7:26	7:44	7:58	8:24	80:8 60:0	0.55 0	10:22	10:56	11:22	11:53		12:22P	12:53	1:22	1:53	2:22	2:53	3:23	3:58	4:28	5:03 5:37	6:03	6:45	7:01	7:42	c 7:50	c 8:20	c 9:05			R.	TAR	c - 10/10		Soute 5			
& 554	Геахе	Waverley Square	1		7:00A	Construction of the local section.	7:30		8:10	0.10	0.10	1010		11:10	••••	00000000	12:10P	1	1:10		2:10		3:10	10000 - FOOT STOLES	4:15	1 5-20		t 6:28		t.7:25	1		1								hote	ci iono	diman.
553		Leave Roberts	3:25A	3:50		7:15		7:45	: :	3:45	 3-45	2	1.45		1:40			2:40P		1:40		2:40		3:45			5:50		6:50		1	1	1								۵	< 3	;

Roberts Waltham-7:30 10:10 t7255 | | | | 7:00A 8:10 9:10 11:10 12:10P 1:10 2:10 3:10 4:15 t 5:20 t 6:28 Leave Waverley Square ł I 6:25A 6:50 7:15 7:15 7:45 8:45 8:45 9:45 9:45 12:40P Leave Roberts 6:50 6:50 1:40 1:40 2:40 3:45 Arrive Central Sq. Wattham The 505 route is not intended for local non-highway travel. Inbound bus stops before the route enters the highway are pickup only. Outound bus stops after the route exits the highway are dropoff only. For local travel, please use Route 553, 554, or 558. 6:26A 7:17 7:17 7:17 7:16 7:16 8:12 8:12 8:12 8:12 8:12 9:12 9:12 9:35 Outbound 6:18A 7:26 7:24 8:18 8:18 8:18 8:18 8:18 8:18 9:24 9:24 9:24 9:24 Arrive West Newton Outer Express Bus-Central Square, Waltham-Downtown Boston No Route 505 service on weekends Leave Federal 8 Franklin 6:02A 6:31 7:05 7:23 7:24 7:28 8:18 8:18 8:18 9:05 9:05 Route 505 Arrive Federal & Franklin 4:30P 5:07 5:30 5:30 6:26 6:25 6:35 6:35 6:35 7:21 6:29A 6:44 6:59 6:54 6:54 8:55 8:55 8:55 9:11 9:22 9:22 9:22 9:22 9:22 9:22 10:26 10:26 10:26 punoqui 4:09P 5:23 5:23 6:15 6:37 7:03 7:03 Arrive Merican Arrive A Callerative Mailtansve S:S5A S S:S5A S S S

357P 453 5510 5529 5529 5529 5529 5529 5529 5529 553 6538 6538

505

Weekday

Sight Line Analysis

Stopping Sight Distance - Posted

		SPEED (MPH)	BRAKE REACTION DISTANCE (FT)	BRAKING DISTANCE (FT)	CALCULATED STOPPING SIGHT DISTANCE (FT)
Direction 1	NB	25	91.875	59.9	151.8
Direction 2	SB	25	91.875	59.9	151.8

INPUTS	Direction 1	Direction 2
Travel Direction	NB	SB
Speed	25	25
Grade	0	0
t	2.5	2.5
а	. 11.2	11.2

Stopping Sight Distance (SSD) - Source: AASHTO

SSD = Reaction Distance + Brake Distance

Reaction Distance = 1.47 x t x V

Brake Distance = V^2 / (30 x ((a/32.2)+G))

Where:

t = reaction time (sec)

V = travel speed (mph) G= roadway grade a - deceleration rate (ft/sec^2)

Stopping Sight Distance - 85th Percentile

		SPEED (MPH)	BRAKE REACTION DISTANCE (FT)	BRAKING DISTANCE (FT)	CALCULATED STOPPING SIGHT DISTANCE (FT)
Direction 1	NB	29	106.575	80.6	187.2
Direction 2	SB	29	106.575	80.6	187.2

INPUTS	Direction 1	Direction 2
Travel Direction	NB	SB
Speed	29	29
Grade	0	0
t	2.5	2.5
а	11.2	11.2

Stopping Sight Distance (SSD) - Source: AASHTO SSD = Reaction Distance + Brake Distance Reaction Distance = 1.47 x t x V Brake Distance = V^2 / (30 x ((a/32.2)+G)) Where: t = reaction time (sec) V = travel speed (mph) G= roadway grade a - deceleration rate (ft/sec^2)

Intersection Sight Distance Calculations

Source: A Policy on Geometric Design of Highways and Street, 6th Edition; AASHTO; 2011.

Passenger Car ISD = 1.47 * V * t

V = speed t = time gap

t = 7.5 s for a passenger car for Left Turn from a Stop t = 6.5 s for a passenger car for Right Turn from a Stop

Posted (Regulatory) Speed Limit

Lexington Street North ISD = 1.47 * 25 * 7.5 = 276 ft SAY 280 ft (left-turn from a stop)

Lexington Street South ISD = 1.47 * 25 * 6.5 = 239 ft SAY 240 ft (right-turn from a stop)

Background Growth

	STATION 691	- QUINCY - R	TE.I-93 - NOF	TH OF RTE	28								
g	JAN 173 000	FEB 175,000	MAR 177 607	APR 104 334	MAY 106 P34		JUL	AUG	SEP 400 per	OCT	NON	DEC	YEAR
3	-2%	%0	4%	-1%	-1%	%0	-1%	-1%	130,000	160,291	600'0/I	1/4,000	180,197 0.5%
11	166,541	175,019	190,696	192,155	193,034	197,594	193,303	191,197	193,140	188,694	187,378	187,895	188,054
12	-2%	6% 185.226	0% 190.193	0% 192 337	1% 194 846	-1% 195 145	-1% 191 419	3% 196 457	-1% 190 548	-2% 185.600	0% 186 /60	-3%	-0.1%
ţ	%6	-1%	-5%	-3%	-1%	%0	%0	1%	%0	2%	-1%	-3%	-0.1%
13	179,468	182,613	180,861	187,402	193,159 110	194,612	192,130	197,467	191,411	190,128	185,233	176,163	187,554
14	165,955	170,581	187,003	193,263	194,348	198,176	193,591	197,456	193,827	192,895	0% 185,667	5% 185,147	0.2% 188,159
u T	3%	%2-	~8- %8-	-10%	%8- %8-	-13%	%E-	3%	3%	2%	4%	4%	-1.4%
2	4%	775'ACI.	067'L/L	BL2, P11	1/8,128 7%	1/2,060	18/,0/1 5%	202,569 1%	198,773 1%	197,111	192,381 1%	192,770	183,069 3,8%
17	185,127	189,054	199,012	199,259	202,004	181,236	205,446	207,586	200,920	199,524	198,080	194,984	196,853
Seasonal Adjustment Factor (to average month)	1.09	1.07	1.02	0.99	0.98	0.99	0.97	0.95	0.97	0.98	1.01	1.02 Growth	70470
	STATION 703	ABINGTON	- PTE 133 - 1	ИТ ТИБ ВОО									0,11.0
YR	NAL		MAR	APR	MAY	NUL	JUL	AUG	SEP	OCT	NON	DEC	YEAR
60	12,251	13,199 200	13,301	13,860	13,231	13,817	13,354	13,212	14,037	13,712	13,161	13,327	13,372
10	12,196	13,134	13,560	14,051	5% 13,835	13,900	u% 13,353	13,338	-1% 13,928	0% 13,733	2% 13,414	-1%	0.8% 13,472
	-5%	~4% 77	-1%	-4%	-3%	-2%	-3%	-2%	-1%	-2%	%0	1%	-2.0%
11	11,629 5%	12,651 4%	13,451 0%	13,518 -1%	13,476 0%	13,655 -1%	12,907 -6%	13,088 0%	13,778 2%	13,495 1%	13,434 0%	13,377	13,205 -0.3%
12	12,181	13,151	13,410	13,379	13,452	13,479	12,127	13,103	13,441	13,679	13,452	13,136	13, 166
13	12 347	-6%	-4% 12 R70	2% 13 501	0% %0	-1%	7% 17 064	13 OE1	0%0 40 467	0% 43 776	-2%	%0 %0	-0.3%
2	4%	3%	3%	-2%	-1%	1%	-2%	-1%	-1%	-3%	%E-	13,001	13,121
14	11,894	12,651	13,252	13,385	13,345	13,524	12,759	12,893	13,376	13,379	12,882	13,315	13,055
15	11 974	-5%	-5% 12 649	-2%	0% 13 378	-1%	12 820	0%0 10 011	-1%	-1%	%0 *1	-2%	-1.3%
2	1%	3%	3%	-1%	-2%	1%	-1%	%0	-1%	-1%	-1%	%0 %0	0,1%
16 16	12,035	12,304	13,075	13,076	13,171	13,574	12,742	12,986	13,061	13,140	12,743	12,940	12,904
Seasonal Agjustment Factor (to average month)	60'L	1.04	00.1	0.97	0.98	0.97	1.02	1.01	0.97	0.97	9	1.00 Growth	-0.50%
	STATION 4165	- 1-95/ ROUT	LE 128 SOUT	H OF 1-90									
ΥR	NAU	FEB	MAR	APR	MAY	NUL	JUL	AUG	SEP	OCT	NON	DEC	YEAR
12	130,033 1%	133,659 	138,451 0%	142,034 3%	158,583 	148,787 1 %	138,599	144,999	141,340	146,271 59/	140,898	128,666	141,027
13	131,812	125,662	138,122	145,780	147,000	149,925	151,813	149,393	150,507	153,009	143,498	130,116	143,053
Ţ	-5%	1%	%E	3%	3%	3%	-5%	%0	1%	-1%	-1%	%9 	0.6%
t	9%9	1%	142,024	671 YOCI	0/c'ici	1%,	1%	143,503	850'ICI	152,148	C/B,141	13/,157 0%	143,974
16	139,436	130,154	148,054	149,295	153,957	156,496	147,414	151,081	152,186	154,663	146,935	137,768	147,287
17	-3% 134.884	0% 130.641	-12% 129.731	-3% 144 492	0% 153 434	0% 156 333	0% 147 RR4	-1%	154 2B1	155.618	149 129	147 141	-0.8% 146.057
Seasonal Adjustment Factor	1.09	1.12	1.04	0.99	0.94	0.94	0.99	26.0	0.96	0.95	1.00	1.06	100-01-1
(to average monut)		:										Growth	0.60%
ΥR	STATION 625	5 - WEYMOU	TH - RTE.3 - 1 MAR	VORTH OF R	ТЕ.18 М∆Ү	NI	88		CED	LUU	NON		VEAD
60	120,200	123,983	124,807	134,354	135,239	143,114	143,685	144,937	140,079	137,288	138,708	136,428	135,235
10	4% 125,304	3% 127,637	6% 132,301	-1% 133,124	0% 135,880	-1% 141,633	-1% 141.706	-2% 142.327	-3% 135.767	-3% 133.473	-1% 137.526	-7% 127.100	-0.6% 134.482
	-3%	-1%	-1%	-6%	%0	%0	-1%	%0	-1%	-2%	-3%	-1%	-1.5%
12	118,936 4%	125,494 -7%	129,712 -4%	116,911 13%	136,235 0%	140,277	139,048 1%	142,140 0%	132,674 1%	128,923 4%	129,593 1%	125,409	130,446
13	123,783	116,501	124,813	131,533	136,712	138,977	140,057	141,851	133,978	134,144	128,712	124,607	131,306
14	113.701	118439	2% 127037	131150	-1%	0% 139,606	5% 147,748	4% 147,593	2% 136,789	-1%	11% 143.498	4% 130 116	0.9% 133.623
ç	3%	1%	1%	1%	1%	1%	-2%	-2%	%0	1%	-5%	%0	-0.2%
9	120,926	121003 3%	128951 0%	132915 1%	138,071	142,406 0%	140,685 ~1%	142,991 -1%	135,630 -1%	134,163 -1%	129,976 1%	128,837 0%	133,046 0.1%
17 Seasonal Adjustment Factor	124,154 1.10	124154 1.09	129045 1.04	134625 1.02	137,743 0.98	142,253 0.94	139,660 0.94	141,524 0.93	134,110 0.98	133,079	131,317 0.99	128,775	133,370
(in average monimul		4		ļ			:					Growth	-0.16%
Average Seasonal Adjustment Factor /to averane month)	1.09	1.08	MAK 1.02	АРК 0.99	МАҮ 0.97	NUL 96.0	JUL 0.98	AUG 0.96	SEF 0.97	0.98	1.00	DEC 1.03	

ITALICS - ESTIMATED DATA MADT

> Average Yearly Growth Calculated 0.15 Yearly Growth Factor Used 0.55

> > Page 1 of 1

	Medical	Storage	Total
Enter	12	7	19
Exit	3	4	7
Total	15	11	26



Weekday Morning Peak Hour



Date: December 2018 Dwg No. 888 MR01.dwg Copyright © by MDM Transportation Consultants, Inc. All rights reserved. Site Generated Trips Weekday Peak Hour Traffic Volumes

Institute of Transportation Engineers (ITE) 10th Edition Land Use Code (LUC) 151 - Mini Warehousing

Average Vehicle Trips Ends vs: Independent Variable (X):	1000 Sq. Feet Gross F 107.397	loor Area
AVERAGE WEEKDAY DAILY		
T = 1.51 * (X)		
T = 1.51 * 107.397		
T = 162.17		
T = 162 vehicle trips		
with 50% (81 vpd) er	itering and 50% (81	vpd) exiting.
	0	1 / 0
WEEKDAY MORNING PEAK HOUR OF	ADJACENT STREET TRAFFIC	
T = 0.10 * (X)		
T = 0.10 * 107.397		
T = 10.74		
T = 11 vehicle trips		
with 60% (7 vph) er	tering and 40% (4	vph) exiting.
WEEKDAY EVENING PEAK HOUR OF A	ADJACENT STREET TRAFFIC	
T = 0.17 * (X)		
T = 0.17 * 107.397		
T = 18.26		
T = 18 vehicle trips		
with 47% (8 vph) er	tering and 53% (10	vph) exiting.
SATURDAY DAILY		
T = 1.95 * (X)	(Small Sample Si	ize - Use with Caution)
$T = 1.95^*$ 107.397		
T = 209.42		
T = 210 vehicle trips		
with 50% (105 vpd) er	tering and 50% (105	vpd) exiting.
SATURDAY MIDDAY PEAK HOUR OF	Generator	
T = 0.31 * (X)	(Small Sample Si	ize - Use with Caution)
T = 0.31 * 107.397		
T = 33.29		

T = 33 vehicle trips

with 59% (19 vph) entering and 41% (14 vph) exiting.

Institute of Transportation Engineers (ITE) 10th Edition Land Use Code (LUC) 720 - Medical-Dental Office Building

Average Vehicle Trips Ends vs:1000 Sq. Feet Gross Floor AreaIndependent Variable (X):5.52

AVERAGE WEEKDAY DAILY

T = 34.80 * (X) T = 34.80 * 5.52 T = 192.10 T = 192 vehicle trips with 50% (96 vpd) entering and 50% (96 vpd) exiting.

WEEKDAY MORNING PEAK HOUR OF ADJACENT STREET TRAFFIC

 $T = 2.78^{*} (X)$ $T = 2.78^{*} 5.52$ T = 15.35 T = 15 vehicle tripswith 79% (12 vpd) entering and 21% (3 vpd) exiting.

WEEKDAY EVENING PEAK HOUR OF ADJACENT STREET TRAFFIC

 $\begin{array}{ll} T = 3.46^{*} & (X) \\ T = 3.46^{*} & 5.52 \\ T = 19.10 \\ T = 19 & \text{vehicle trips} \\ \text{with 28\%} (5 & \text{vpd}) \text{ entering and 72\%} (14 & \text{vpd}) \text{ exiting.} \end{array}$

SATURDAY DAILY

T = 8.57 * (X)	(Small Sample Size - Use with Caution)
T = 8.57 * 5.52	
T = 47.31	
T = 48 vehicle trips	
with 50% (24 vpd) entering and 50% (24 vpd) exiting.

SATURDAY MIDDAY PEAK HOUR OF GENERATOR

T = 3.10 * (X)	(Small Sample Size - Use with Caution)
T = 3.10 * 5.52	
T = 17.11	
T = 17 vehicle trips	
with 57% (10 vph) entering and 43% (7 vph) exiting.

□ Trip Generation Calculations

Institute of Transportation Engineers (ITE) 10th Edition Land Use Code (LUC) 210 - Single-Family Detached Housing

Average Vehicle Trips Ends vs:Dwelling UnitsIndependent Variable (X):1

AVERAGE WEEKDAY DAILY

 $\begin{array}{ll} T = 9.5^{*} \ (X) \\ T = 9.5^{*} & 1 \\ T = 9.50 \\ T = 10 & \text{vehicle trips} \\ \text{with 50\%} \ (& 5 & \text{vpd}) \text{ entering and 50\%} \ (& 5 & \text{vpd}) \text{ exiting.} \end{array}$

WEEKDAY MORNING PEAK HOUR OF ADJACENT STREET TRAFFIC

 $\begin{array}{ll} T = 0.74^{*} \mbox{ (X)} \\ T = 0.74^{*} & 1 \\ T = 0.74 \\ T = 1 & \mbox{vehicle trips} \\ \mbox{with 25\% (} & 0 & \mbox{vph) entering and 75\% (} & 1 & \mbox{vph) exiting.} \end{array}$

WEEKDAY EVENING PEAK HOUR OF ADJACENT STREET TRAFFIC

 $\begin{array}{ll} T = 0.99^{*} \ (X) \\ T = 0.99^{*} & 1 \\ T = 0.99 \\ T = 1 & \mbox{vehicle trips} \\ \mbox{with 63\%} \ (& 1 & \mbox{vph}) \ \mbox{entering and 37\%} \ (& 0 & \mbox{vph}) \ \mbox{exiting.} \end{array}$

SATURDAY DAILY

$T = 9.54^{*}(X)$				
T = 9.54*	1			
T = 9.54				
T = 10	vehicle	trips		
with 50% (5	vph) entering and 50% (5	vph) exiting.

SATURDAY MIDDAY PEAK HOUR OF GENERATOR

 $T = 0.93^* (X)$

T = 0.93*

T = 0.93

T = 1 vehicle trips

1

with 54% (1 vph) entering and 46% (0 vph) exiting.
Institute of Transportation Engineers (ITE) 10th Edition Land Use Code (LUC) 220 - Multifamily Housing (Low-Rise)

Average Vehicle Trips Ends vs:Dwelling UnitsIndependent Variable (X):3

AVERAGE WEEKDAY DAILY

WEEKDAY MORNING PEAK HOUR OF ADJACENT STREET TRAFFIC

WEEKDAY MORNING PEAK HOUR OF GENERATOR

 $\begin{array}{ll} T = 0.56 * X \\ T = 0.56 * & 0 \\ T = 1.68 \\ T = 2 & \mbox{vehicle trips} \\ \mbox{with 28\% (1 vph) entering and 72\% (1 vph) exiting.} \end{array}$

WEEKDAY EVENING PEAK HOUR OF ADJACENT STREET TRAFFIC

WEEKDAY EVENING PEAK HOUR OF GENERATOR

 $\begin{array}{ll} T = 0.67 * X \\ T = 0.67 * & 0 \\ T = 2.01 \\ T = 2 & \mbox{vehicle trips} \\ \mbox{with 59\% (1 vph) entering and 41\% (1 vph) exiting.} \end{array}$

SATURDAY DAILY

SATURDAY MIDDAY PEAK HOUR OF GENERATOR

 $\begin{array}{l} T = 0.70 * X \\ T = 0.70 * 3 \\ T = 2.10 \\ T = 2 \\ \text{ wehicle trips} \\ \text{with } 49\% (1 \text{ vph}) \text{ entering and } 51\% (1 \text{ vph}) \text{ exiting.} \end{array}$

Institute of Transportation Engineers (ITE) 10th Edition Land Use Code (LUC) 220 - Multifamily Housing (Low-Rise)

Average Vehicle Trips Ends vs:Dwelling UnitsIndependent Variable (X):24

AVERAGE WEEKDAY DAILY

T = 7.32 * X T = 7.32 * 24 T = 175.68 T = 176 vehicle tripswith 50% (88 vpd) entering and 50% (88 vpd) exiting.

WEEKDAY MORNING PEAK HOUR OF ADJACENT STREET TRAFFIC

T = 0.46 * X T = 0.46 * 24 T = 11.04 T = 11 vehicle tripswith 23% (3 vph) entering and 77% (8 vph) exiting.

WEEKDAY EVENING PEAK HOUR OF ADJACENT STREET TRAFFIC

 $\begin{array}{ll} T = 0.56 * X \\ T = 0.56 * & 24 \\ T = 13.44 \\ T = 13 & \text{vehicle trips} \\ \text{with 63\%} (8 \text{ vph}) \text{ entering and 37\%} (5 \text{ vph}) \text{ exiting.} \end{array}$

SATURDAY DAILY

T = 8.14 * X T = 8.14 * 24 T = 195.36 T = 196 vehicle tripswith 50% (98 vpd) entering and 50% (98 vpd) exiting.

SATURDAY MIDDAY PEAK HOUR OF GENERATOR

T = 0.70 * X T = 0.70 * 24 T = 16.80 T = 17 vehicle tripswith 49% (8 vph) entering and 51% (9 vph) exiting.

□ Trip Distribution Calculations

Newton, Massachusetts







Scale: Not to Scale

MDM TRANSPORTATION CONSULTANTS, INC. Planners & Engineers Attachments

Trip Distribution Calculation

Capacity Analysis

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LEVEL OF SERVICE METHODOLOGY

Capacity analysis of intersections is developed using the Synchro® computer software, which implements the methods of the 2010 Highway Capacity Manual (HCM). The resulting analysis presents a level-of-service (LOS) designation for individual intersection movements and (for signalized intersections) for the entire intersection. The LOS is a letter designation that provides a qualitative measure of operating conditions based on several factors including roadway geometry, speeds, ambient traffic volumes, traffic controls, and driver characteristics. Since the LOS of a traffic facility is a function of the traffic flows placed upon it, such a facility may operate at a wide range of LOS, depending on the time of day, day of week, or period of year. A range of six levels of service are defined on the basis of average delay, ranging from LOS A (the least delay) to LOS F (delays greater than 50 seconds for unsignalized movements, and greater than 80 seconds for signalized movements).

Signalized Intersection Performance Measures

The six LOS designations for signalized intersections may be described as follows:

- *LOS A* describes operations with low control delay; most vehicles do not stop at all.
- *LOS B* describes operations with relatively low control delay. However, more vehicles stop than LOS A.
- *LOS C* describes operations with higher control delays. Individual cycle failures may begin to appear. The number of vehicles stopping is significant at this level, although many still pass through the intersection without stopping.
- *LOS D* describes operations with control delay in the range where the influence of congestion becomes more noticeable. Many vehicles stop and individual cycle failures are noticeable.
- *LOS E* describes operations with high control delay values. Individual cycle failures are frequent occurrences.
- *LOS F* describes operations with high control delay values that often occur with over-saturation. Poor progression and long cycle lengths may also be major contributing causes to such delay levels.

The LOS for signalized intersections are calculated using the operational analysis methodology of the 2010 *Highway Capacity Manual.*¹ This method assesses the effects of signal type, timing, phasing, and progression; vehicle mix; and geometrics on delay. LOS designations are based on the criterion of control or signal delay per vehicle. Control or signal delay is a measure of driver discomfort, frustration, and fuel consumption, and includes initial deceleration delay approaching the traffic signal, queue move-up time, stopped delay and final acceleration delay. **Table A1** summarizes the relationship between LOS and control delay. The tabulated control delay criterion may be applied in assigning LOS designations to individual lane groups, to individual intersection approaches, or to entire intersections.

Table A1 LEVEL-OF-SERVICE CRITERIA FOR SIGNALIZED INTERSECTIONS¹

	Control (Signal) Delay per Vehicle
Level of Service	(Seconds)
А	<u>≤</u> 10.0
В	10.1 to 20.0
С	20.1 to 35.0
D	35.1 to 55.0
Е	55.1 to 80.0
F	>80.0

¹Source: *Highway Capacity Manual 2010;* Transportation Research Board; Washington, DC; 2010.

¹Highway Capacity Manual 2010; Transportation Research Board; Washington, DC; 2010.

Unsignalized Intersection Performance Measures

The six LOS designations for unsignalized intersections may be described as follows:

- LOS A represents a condition with little or no control delay to minor street traffic.
- LOS B represents a condition with short control delays to minor street traffic.
- LOS C represents a condition with average control delays to minor street traffic.
- LOS D represents a condition with long control delays to minor street traffic.
- *LOS E* represents operating conditions at or near capacity level, with very long control delays to minor street traffic.
- *LOS F* represents a condition where minor street demand volume exceeds capacity of an approach lane, with extreme control delays resulting.

The LOS designations of unsignalized intersections are determined by application of a procedure described in the 2010 *Highway Capacity Manual.*² LOS is measured in terms of average control delay. Mathematically, control delay is a function of the capacity and degree of saturation of the lane group and/or approach under study and is a quantification of motorist delay associated with traffic control devices such as traffic signals and STOP signs. Control delay, queue move-up time, and final acceleration delay from a stopped condition. Definitions for LOS at unsignalized intersections are also given in the *Highway Capacity Manual 2010*. **Table A2** summarizes the relationship between LOS and average control delay.

Table A2 LEVEL-OF-SERVICE CRITERIA FOR UNSIGNALIZED INTERSECTIONS¹

	Level o	f Service
Average Control Delay (seconds per vehicle)	v/c≤1	v/c > 1
≤ 10.0	А	F
10.1 to 15.0	В	F
15.1 to 25.0	С	F
25.1 to 35.0	D	F
35.1 to 50.0	Е	F
>50.0	F	F

¹Source: *Highway Capacity Manual* 2010, Transportation Research Board; Washington, DC; 2010.

	۶	+	*	4		×	-	1	1	1	Ļ	
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			र्स	1		4			\$	
Volume (vph)	30	59	47	59	49	123	67	315	51	203	521	20
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width (ft)	15	15	15	12	12	11	12	12	12	12	12	12
Storage Length (ft)	0		0	0		30	0		0	0		0
Storage Lanes	0		0	0		1	0		0	0		0
Taper Length (ft)	25			25			25			25		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.953				0.850		0.984			0.996	
FIt Protected		0.989			0.973			0.992			0.987	
Satd. Flow (prot)	0	1716	0	0	1732	1473	0	1760	0	0	1758	0
Flt Permitted		0.909			0.747			0.809			0.757	
Satd. Flow (perm)	0	1577	0	0	1330	1473	0	1435	0	0	1349	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		32				134		19			4	
Link Speed (mph)		30			30			30			30	
Link Distance (ft)		1000			1000			1000			600	
Travel Time (s)		22.7			22.7			22.7			13.6	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	33%	10%	9%	9%	4%	6%	2%	6%	6%	9%	5%	10%
Adj. Flow (vph)	33	64	51	64	53	134	73	342	55	221	566	22
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	148	0	0	117	134	0	470	0	0	809	0
Enter Blocked Intersection	No											
Lane Alignment	Left	Left	Right									
Median Width(ft)		0	•		0	-		0			0	
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane												
Headway Factor	0.88	0.88	0.88	1.00	1.00	1.04	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		9	15		9	15		9	15		9
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		
Minimum Split (s)	20.0	20.0		20.0	20.0	20.0	55.0	55.0		55.0	55.0	
Total Split (s)	20.0	20.0		20.0	20.0	20.0	55.0	55.0		55.0	55.0	
Total Split (%)	26.7%	26.7%		26.7%	26.7%	26.7%	73.3%	73.3%		73.3%	73.3%	
Maximum Green (s)	15.0	15.0		15.0	15.0	15.0	50.0	50.0		50.0	50.0	
Yellow Time (s)	4.0	4.0		4.0	4.0	4.0	4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	1.0		1.0	1.0	1.0	1.0	1.0		1.0	1.0	
Lost Time Adjust (s)		0.0			0.0	0.0		0.0			0.0	
Total Lost Time (s)		5.0			5.0	5.0		5.0			5.0	
Lead/Lag												
Lead-Lag Optimize?												
Act Effct Green (s)		15.0			15.0	15.0		50.0			50.0	
Actuated g/C Ratio		0.20			0.20	0.20		0.67			0.67	
v/c Ratio		0.43			0.44	0.33		0.49			0.90	
Control Delay		25.0			32.4	7.8		8.0			26.3	
Queue Delay		0.0			0.0	0.0		0.0			0.0	

G:\Projects\888 - Newton (Capasso)\Synchro\Ex AM.syn MDM Transportation Consultants, Inc.

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Total Delay		25.0			32.4	7.8		8.0			26.3	
LOS		С			С	А		А			С	
Approach Delay		25.0			19.3			8.0			26.3	
Approach LOS		С			В			А			С	
Queue Length 50th (ft)		47			48	0		87			265	
Queue Length 95th (ft)		100			97	42		149			#565	
Internal Link Dist (ft)		920			920			920			520	
Turn Bay Length (ft)						30						
Base Capacity (vph)		341			266	401		963			900	
Starvation Cap Reductn		0			0	0		0			0	
Spillback Cap Reductn		0			0	0		0			0	
Storage Cap Reductn		0			0	0		0			0	
Reduced v/c Ratio		0.43			0.44	0.33		0.49			0.90	
Intersection Summary												
Area Turas	Other											

 Area Type:
 Other

 Cycle Length: 75
 Actuated Cycle Length: 75

 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

 Natural Cycle: 75

 Control Type: Pretimed

 Maximum v/c Ratio: 0.90

 Intersection Signal Delay: 20.0

 Intersection Capacity Utilization 90.0%

 ICU Level of Service E

 Analysis Period (min) 15

 # 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

ø2 (R)	→ _{Ø4}
55-5	20 s
■ ▼ ² ø6 (R)	₩ ₩ ø8
55 S	20 s

Intersection								
Int Delay, s/veh (D.1							
Movement	WBL	WBR		NBT	NBR	SBL	SBT	
Vol, veh/h	5	4		513	1	2	544	
Conflicting Peds, #/hr	0	0		0	0	0	0	
Sign Control	Stop	Stop		Free	Free	Free	Free	
RT Channelized	-	None		-	None	-	None	
Storage Length	0	-		-	-	-	-	
Veh in Median Storage, #	0	-		0	-	-	0	
Grade, %	0	-		0	-	-	0	
Peak Hour Factor	98	98		98	98	98	98	
Heavy Vehicles, %	0	0		6	0	0	5	
Mvmt Flow	5	4		523	1	2	555	
Maior/Minor	Minor1			Maior1		Maior2		
Conflicting Flow All	1083	524		0	0	524	0	
Stage 1	524			-	-	-	-	
Stage 2	559	-		-	-	-	-	
Critical Hdwy	64	62		-	-	4.1	-	
Critical Hdwy Stg 1	54	-		-	-	-	-	
Critical Hdwy Stg 2	5.4	-		-	-	-	-	
Follow-up Hdwy	3.5	33		-	-	2.2	-	
Pot Can-1 Maneuver	243	557		-	-	1053	-	
Stage 1	598	-		-	-	-	-	
Stage 2	576	-		-	-	-	-	
Platoon blocked %	0,0			-	-		-	
Mov Cap-1 Maneuver	242	557		-	-	1053	-	
Mov Cap-2 Maneuver	242	-		-	-	-	-	
Stage 1	598	-		-	-	-	-	
Stage 2	574	-		-	-	-	-	
olago 1	07.							
Annroach	WR			NR		SB		
HCM Control Delay	16.5			0		0		
HCM LOS	10.5			U		0		
	0							
Minor Lane/Maior Mymt	NBT	NBRWBLn1	SBL	SBT				
Canacity (veh/h)		- 323	1053					
HCM Lane V/C Ratio	_	- 0.028	0.002	-				
HCM Control Delay (s)	-	- 16.5	8.002	0				
HCM Lane LOS	-	- C	Δ	Ă				
	-	0	11					

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HCM 95th %tile Q(veh)

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- 0.1

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			र्भ	7		\$			\$	
Volume (vph)	28	64	100	76	57	119	29	449	42	182	392	21
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width (ft)	15	15	15	12	12	11	12	12	12	12	12	12
Storage Length (ft)	0		0	0		30	0		0	0		0
Storage Lanes	0		0	0		1	0		0	0		0
Taper Length (ft)	25			25			25			25		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.930				0.850		0.989			0.995	
Fit Protected		0.993			0.972			0.997			0.985	
Satd. Flow (prot)	0	1854	0	0	1754	1531	0	1829	0	0	1838	0
Flt Permitted		0.937			0.619			0.954			0.718	
Satd. Flow (perm)	0	1749	0	0	1117	1531	0	1750	0	0	1340	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		65				119		13			5	
Link Speed (mph)		30			30			30			30	
Link Distance (ft)		1000			1000			1000			600	
Travel Time (s)		22.7			22.7			22.7			13.6	
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Heavy Vehicles (%)	0%	3%	6%	1%	11%	2%	10%	2%	2%	2%	1%	1%
Adj. Flow (vph)	29	67	104	79	59	124	30	468	44	190	408	22
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	200	0	0	138	124	0	542	0	0	620	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)		0			0			0			0	
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane												
Headway Factor	0.88	0.88	0.88	1.00	1.00	1.04	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		9	15		9	15		9	15		9
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		
Minimum Split (s)	20.0	20.0		20.0	20.0	20.0	55.0	55.0		55.0	55.0	
Total Split (s)	20.0	20.0		20.0	20.0	20.0	55.0	55.0		55.0	55.0	
Total Split (%)	26.7%	26.7%		26.7%	26,7%	26.7%	73.3%	73.3%		73.3%	73.3%	
Maximum Green (s)	15.0	15.0		15.0	15.0	15.0	50.0	50.0		50.0	50.0	
Yellow Time (s)	4.0	4.0		4.0	4.0	4.0	4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	1.0		1.0	1.0	1.0	1.0	1.0		1.0	1.0	
Lost Time Adjust (s)		0.0			0.0	0.0		0.0			0.0	
Total Lost Time (s)		5.0			5.0	5.0		5.0			5.0	
Lead/Lag												
Lead-Lag Optimize?						100		60 0			FO O	
Act Effet Green (s)		15.0			15.0	15.0		50.0			50.0	
Actuated g/C Ratio		0.20			0.20	0.20		0.67			0.67	
v/c Ratio		0.50			0.62	0.31		0.46			0.69	
Control Delay		22.7			41.4	8.4		1.4			12.8	
Queue Delay		0.0			0.0	0.0		0.0			0.0	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Total Delay		22.7			41.4	8.4		7.4			12.8	
LOS		С			D	А		А			В	
Approach Delay		22.7			25.8			7.4			12.8	
Approach LOS		С			С			А			В	
Queue Length 50th (ft)		55			59	2		101			151	
Queue Length 95th (ft)		117			#132	43		160			272	
Internal Link Dist (ft)		920			920			920			520	
Turn Bay Length (ft)						30						
Base Capacity (vph)		401			223	401		1171			895	
Starvation Cap Reductn		0			0	0		0			0	
Spillback Cap Reductn		0			0	0		0			0	
Storage Cap Reductn		0			0	0		0			0	
Reduced v/c Ratio		0.50			0.62	0.31		0.46			0.69	
Intersection Summary										-		
Area Type: (Other											
Cycle Length: 75												
Actuated Cycle Length: 75												
Offset: 0 (0%), Referenced to	phase 2	NBTL and	6:SBTL,	Start of 0	Green							
Natural Cycle: 75												
Control Type: Pretimed												
Maximum v/c Ratio: 0.69												
Intersection Signal Delay: 14	.3			In	tersection	LOS: B						

Intersection Capacity Utilization 116.8% Analysis Period (min) 15

ICU Level of Service H

95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Ø2 (R)	
55 s	20 s
Ø6 (R)	₩ Ø8
95°s	20 s

0.1

Intersection

Int Delay, s/veh

Movement	WBL	WBR		NB	Г	NBR	SBL	SBT	
Vol, veh/h	3	3		62	6	5	5	570	
Conflicting Peds, #/hr	0	0			0	0	0	0	
Sign Control	Stop	Stop		Free	e	Free	Free	Free	
RT Channelized	-	None			-	None	-	None	
Storage Length	0	-			-	-	-	-	
Veh in Median Storage, #	0	-		(0	-	-	0	
Grade, %	0	-		(0	-	-	0	
Peak Hour Factor	98	98		98	В	98	98	98	
Heavy Vehicles, %	0	0			2	0	0	1	
Mvmt Flow	3	3		639	9	5	5	582	
Major/Minor	Minor1			Major	1		Major2		
Conflicting Flow All	1233	641		()	0	644	0	
Stage 1	641	-			-	-		-	
Stage 2	592	-			-	-	-	-	
Critical Hdwy	6.4	6.2			-	-	4.1	-	
Critical Hdwy Stg 1	5.4	-			•	-	-	-	
Critical Hdwy Stg 2	5.4	-			-	-	-	-	
Follow-up Hdwy	3.5	3.3			-	-	2.2	-	
Pot Cap-1 Maneuver	197	478			-	-	951	-	
Stage 1	528	-			-	-	-	-	
Stage 2	557	-			-	-	-	-	
Platoon blocked, %					-	-		-	
Mov Cap-1 Maneuver	195	478			-	-	951	-	
Mov Cap-2 Maneuver	195	-			-	-	-	-	
Stage 1	528	-			-	-	-	-	
Stage 2	553	-			-	-	-	-	
•									
Approach	WB			NE	3		SB		
HCM Control Delay, s	18.3			()		0.1		
HCM LOS	С								
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT					
Capacity (veh/h)		- 277	951	-					
HCM Lane V/C Ratio	-	- 0.022	0.005	-					
HCM Control Delay (s)	-	- 18.3	8.8	0					
HCM Lane LOS	-	- C	А	А					
HCM 95th %tile Q(veh)	-	- 0.1	0	-					
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			र्स	7		\$			\$	
Volume (vph)	34	61	51	60	52	126	76	323	52	208	534	31
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width (ft)	15	15	15	12	12	11	12	12	12	12	12	12
Storage Length (ft)	0		0	0		30	0		0	0		0
Storage Lanes	0		0	0		1	0		0	0		0
Taper Length (ft)	25			25			25			25		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.953				0.850		0.984			0.995	
Fit Protected		0.988			0.974			0.992			0.987	
Satd. Flow (prot)	0	1711	0	0	1735	1473	0	1761	0	0	1756	0
Fit Permitted		0.900			0.734			0.782			0.751	
Satd. Flow (perm)	0	1558	0	0	1307	1473	0	1388	0	0	1336	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		32				137		19			6	
Link Speed (mph)		30			30			30			30	
Link Distance (ft)		1000			1000			1000			600	
Travel Time (s)		22.7			22.7			22.7			13.6	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	33%	10%	9%	9%	4%	6%	2%	6%	6%	9%	5%	10%
Adj. Flow (vph)	37	66	55	65	57	137	83	351	57	226	580	34
Shared Lane Traffic (%)							_		_			
Lane Group Flow (vph)	0	158	0	0	122	137	0	491	0	0	840	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)		0			0			0			0	
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane				4.00	4.00		4.00	4 00	4.00	4 00	4.00	4.00
Headway Factor	0.88	0.88	0.88	1.00	1.00	1.04	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		9	15		9	15		9	15 D		9
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	
Protected Phases		4		•	8	0	0	Z		6	b	
Permitted Phases	4	00.0		8	00.0	8	2 55 0	55.0		55.0	EE 0	
Minimum Split (s)	20.0	20.0		20.0	20.0	20.0	00.U	55.0		55.U	55.0	
Total Split (S)	20.0	20.0		20.0	20.0	20.0	00.U	0.0C 72.20/		0.00	0.00	
Total Split (%)	20.1%	20.7%		20.7%	20.7%	20.7%	13.3%	13.3%		13.3%	13.3%	
Vallau Time (a)	15.0	15.0		10.0	15.0	10.0	0.00	50.0		50.0	50.0	
All Bod Time (s)	4.0	4.0		4.0	4.0	4.0	4.0	4.0		4.0	4.0	
All-Reu Time (S)	1.0	1.0		1.0	1.0	1.0	1.0	1.0		1.0	0.0	
Total Last Time (a)		0.0 E 0			0.0 5.0	0.0 5.0		0.0 5.0			0.0 5.0	
		5.0			5.0	5.0		5.0			5.0	
Lead Log Optimize?												
Act Effet Groop (s)		15.0			15.0	15.0		50.0			50.0	
Actuated a/C Ratio		0.20			0.20	0.20		0.0			0.0	
v/c Ratio		0.20			0.20	0.20		0.07 0.53			0.07	
Control Delay		26.2			33.3	7 R		8.00 8.7			327	
Queue Delay		0.0			0.0	0.0		0.0			0.0	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Total Delay		26.2			33.3	7.8		8.7			32.7	
LOS		С			С	А		А			С	
Approach Delay		26.2			19.8			8.7			32.7	
Approach LOS		С			В			А			С	
Queue Length 50th (ft)		52			51	0		95			297	
Queue Length 95th (ft)		107			101	43		165			#602	
Internal Link Dist (ft)		920			920			920			520	
Turn Bay Length (ft)						30						
Base Capacity (vph)		337			261	404		931			892	
Starvation Cap Reductn		0			0	0		0			0	
Spillback Cap Reductn		0			0	0		0			0	
Storage Cap Reductn		0			0	0		0			0	
Reduced v/c Ratio		0.47			0.47	0.34		0.53			0.94	

Intersection Summary

Area Type: Other Cycle Length: 75 Actuated Cycle Length: 75 Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green Natural Cycle: 80 Control Type: Pretimed Maximum v/c Ratio: 0.94 Intersection Signal Delay: 23.4 Intersection LOS: C Intersection Capacity Utilization 90.3% ICU Level of Service E Analysis Period (min) 15 # 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

g ≪ ¶ g2 (R)	ø₄
55 s	20 s
J ▼ [™] g6 (R)	₩ Ø8
55 s	20 s

HCM 2010 TWSC 2: Lexington Street & Milton Avenue

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	in	cti	rse	te	In

Int Delay, s/veh

Movement	WBL	WBR		NBT	Г	NBR	SBL	SBT	
Vol, veh/h	5	4		529	9	1	2	568	
Conflicting Peds, #/hr	0	0		()	0	0	0	
Sign Control	Stop	Stop		Free	Э	Free	Free	Free	
RT Channelized	-	None			- 1	None	-	None	
Storage Length	0	-			-	-	-	-	
Veh in Median Storage, #	0	-		()	-	-	0	
Grade, %	0	-		()	-	-	0	
Peak Hour Factor	98	98		98	3	98	98	98	
Heavy Vehicles, %	0	0		f	3	0	0	5	
Mymt Flow	5	4		540)	1	2	580	
Major/Minor	Minor1			Major	1		Major2		
Conflicting Flow All	1124	540		()	0	541	0	
Stage 1	540	-			-	-	-	-	
Stage 2	584	-			-	-	-	-	
Critical Hdwy	6.4	6.2			-	-	4.1	-	
Critical Hdwy Stg 1	5.4	-			-	-	-	-	
Critical Hdwy Stg 2	5.4	-			-	-	-	-	
Follow-up Hdwy	3.5	3.3			-	-	2.2	-	
Pot Cap-1 Maneuver	229	546			-	-	1038	-	
Stage 1	588	-			-	-	-	-	
Stage 2	561	-			-	-	-	-	
Platoon blocked, %					-	-		-	
Mov Cap-1 Maneuver	228	546			-	-	1038	-	
Mov Cap-2 Maneuver	228	-			-	-	-	-	
Stage 1	588	-			-	-	-	-	
Stage 2	559	-			-	-	-	-	
Ū									
Approach	WB			NE	3		SB		
HCM Control Delay, s	17			()		0		
HCM LOS	С								
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT					
Capacity (veh/h)	-	- 308	1038	-					
HCM Lane V/C Ratio	-	- 0.03	0.002	-					
HCM Control Delay (s)	-	- 17	8.5	0					
HCM Lane LOS	-	- C	А	А					
HCM 95th %tile Q(veh)	-	- 0.1	0	-					

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			र्स	Ť		\$			\$	
Volume (vph)	41	69	112	78	59	122	35	460	43	187	402	29
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width (ft)	15	15	15	12	12	11	12	12	12	12	12	12
Storage Length (ft)	0		0	0		30	0		0	0		0
Storage Lanes	0		0	0		1	0		0	0		0
Taper Length (ft)	25			25			25			25		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.932				0.850		0.989			0.994	
Fit Protected		0.991			0.972			0.997			0.985	
Satd. Flow (prot)	0	1857	0	0	1754	1531	0	1828	0	0	1836	0
Flt Permitted		0.912			0.575			0.941			0.712	
Satd. Flow (perm)	0	1709	0	0	1038	1531	0	1725	0	0	1327	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		61				118		13			7	
Link Speed (mph)		30			30			30			30	
Link Distance (ft)		1000			1000			1000			600	
Travel Time (s)		22.7			22.7			22.7			13.6	
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Heavy Vehicles (%)	0%	3%	6%	1%	11%	2%	10%	2%	2%	2%	1%	1%
Adj. Flow (vph)	43	72	117	81	61	127	36	479	45	195	419	30
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	232	0	0	142	127	0	560	0	0	644	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)		0			0			0			0	
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane												
Headway Factor	0.88	0.88	0.88	1.00	1.00	1.04	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		9	15		9	15		9	15		9
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	
Protected Phases		4			8			2		_	6	
Permitted Phases	4			8		8	2			6		
Minimum Split (s)	20.0	20.0		20.0	20.0	20.0	55.0	55.0		55.0	55.0	
Total Split (s)	20.0	20.0		20.0	20.0	20.0	55.0	55.0		55.0	55.0	
Total Split (%)	26.7%	26.7%		26.7%	26.7%	26.7%	73.3%	73.3%		73.3%	73.3%	
Maximum Green (s)	15.0	15.0		15.0	15.0	15.0	50.0	50.0		50.0	50.0	
Yellow Time (s)	4.0	4.0		4.0	4.0	4.0	4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	1.0		1.0	1.0	1.0	1.0	1.0		1.0	1.0	
Lost Time Adjust (s)		0.0			0.0	0.0		0.0			0.0	
Total Lost Time (s)		5.0			5.0	5.0		5.0			5.0	
Lead/Lag												
Lead-Lag Optimize?												
Act Effct Green (s)		15.0			15.0	15.0		50.0			50.0	
Actuated g/C Ratio		0.20			0.20	0.20		0.67			0.67	
v/c Ratio		0.59			0.69	0.32		0.49			0.73	
Control Delay		27.0			47.3	8.8		7.7			14.0	
Queue Delay		0.0			0.0	0.0		0.0			0.0	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Total Delay		27.0			47.3	8.8		7.7			14.0	
LOS		С			D	А		А			В	
Approach Delay		27.0			29.1			7.7			14.0	
Approach LOS		С			С			А			В	
Queue Length 50th (ft)		71			62	3		106			163	
Queue Length 95th (ft)		142			#144	45		170			300	
Internal Link Dist (ft)		920			920			920			520	
Turn Bay Length (ft)						30						
Base Capacity (vph)		390			207	400		1154			887	
Starvation Cap Reductn		0			0	0		0			0	
Spillback Cap Reductn		0			0	0		0			0	
Storage Cap Reductn		0			0	0		0			0	
Reduced v/c Ratio		0.59			0.69	0.32		0.49			0.73	
Intersection Summary												
Area Type:	Other											
Cycle Length: 75												
Actuated Cycle Length: 75	5											
Offset: 0 (0%), Referenced	d to phase 2	NBTL and	l 6:SBTL,	Start of (Green							
Natural Cycle: 75												
Control Type: Pretimed												
Maximum v/c Ratio: 0.73												
Intersection Signal Delay:	16.1			In	tersectior	I LOS: B						
Intersection Capacity Utiliz	zation 115.39	%		IC	CU Level o	of Service	Н					

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

ø2 (R)	▲ ₀₄
55 S	20 s
∎ ▼ [™] ø6 (R)	₩ Ø8
55 s	20 s

0.1

Intersection

Int Delay, s/veh

Movement	WBL	WBR	_	NBT	N	BR	SBL	SBT	
Vol, veh/h	3	3		654	•	5	5	591	
Conflicting Peds, #/hr	0	0		0)	0	0	0	
Sign Control	Stop	Stop		Free	FI	ree	Free	Free	
RT Channelized	-	None		-	No	one	-	None	
Storage Length	0	-		-		-	-	-	
Veh in Median Storage, #	0	-		0		-	-	0	
Grade, %	0	-		0		-	-	0	
Peak Hour Factor	98	98		98		98	98	98	
Heavy Vehicles, %	0	0		2		0	0	1	
Mvmt Flow	3	3		667		5	5	603	
Major/Minor	Minor1		-	Major1			Major2		
Conflicting Flow All	1283	670		0		0	672	0	
Stage 1	670	-		-		-	-	-	
Stage 2	613	-		-		-	-	-	
Critical Hdwy	6.4	6.2		-		-	4.1	-	
Critical Hdwy Stg 1	5.4	-		-		-	-	-	
Critical Hdwy Stg 2	5.4	-		-		-	-	-	
Follow-up Hdwy	3.5	3.3		-	,	-	2.2	-	
Pot Cap-1 Maneuver	184	460		-		-	928	-	
Stage 1	512	-		-	,	-	-	-	
Stage 2	544	-		-		-	-	-	
Platoon blocked, %				-		-		-	
Mov Cap-1 Maneuver	183	460		-		-	928	-	
Mov Cap-2 Maneuver	183	-		-		-	-	-	
Stage 1	512	-		-		-	-	-	
Stage 2	540	-		-		-	-	-	
-									
Approach	WB			NB			SB		
HCM Control Delay, s	19.1			0			0.1		
HCM LOS	С								
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT					
Capacity (veh/h)	-	- 262	928	-					
HCM Lane V/C Ratio	-	- 0.023	0.005	-					
HCM Control Delay (s)	-	- 19.1	8.9	0					
HCM Lane LOS	-	- C	А	А					
HCM 95th %tile Q(veh)	-	- 0.1	0	-					

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			र्भ	7		4			\$	
Volume (vph)	34	61	51	60	52	126	76	324	52	209	536	32
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width (ft)	15	15	15	12	12	11	12	12	12	12	12	12
Storage Length (ft)	0		0	0		30	0		0	0		0
Storage Lanes	0		0	0		1	0		0	0		0
Taper Length (ft)	25			25			25			25		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.953				0.850		0.984			0.994	
Flt Protected		0.988			0.974			0.992			0.987	
Satd. Flow (prot)	0	1711	0	0	1735	1473	0	1761	0	0	1754	0
Flt Permitted		0.900			0.734			0.781			0.750	
Satd. Flow (perm)	0	1558	0	0	1307	1473	0	1386	0	0	1333	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		32				137		19			6	
Link Speed (mph)		30			30			30			30	
Link Distance (ft)		1000			1000			1000			600	
Travel Time (s)		22.7			22.7			22.7			13.6	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Heavy Vehicles (%)	33%	10%	9%	9%	4%	6%	2%	6%	6%	9%	5%	10%
Adj. Flow (vph)	37	66	55	65	57	137	83	352	57	227	583	35
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	158	0	0	122	137	0	492	0	0	845	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)		0			0			0			0	
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane												
Headway Factor	0.88	0.88	0.88	1.00	1.00	1.04	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		9	15		_ 9	15		9	15		9
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	
Protected Phases		4		_	8	_	_	2			6	
Permitted Phases	4			8		8	2			6		
Minimum Split (s)	20.0	20.0		20.0	20.0	20.0	55.0	55.0		55.0	55.0	
Total Split (s)	20.0	20.0		20.0	20.0	20.0	55.0	55.0		55.0	55.0	
Total Split (%)	26.7%	26.7%		26.7%	26.7%	26.7%	73.3%	73.3%		/3.3%	/3.3%	
Maximum Green (s)	15.0	15.0		15.0	15.0	15.0	50.0	50.0		50.0	50.0	
Yellow Time (s)	4.0	4.0		4.0	4.0	4.0	4.0	4.0		4.0	4.0	
All-Red Time (s)	1.0	1.0		1.0	1.0	1.0	1.0	1.0		1.0	1.0	
Lost Time Adjust (s)		0.0			0.0	0.0		0.0			0.0	
Total Lost Time (s)		5.0			5.0	5.0		5.0			5.0	
Lead/Lag												
Lead-Lag Optimize?					45.0	45.0		50 0			FA A	
Act Effect Green (s)		15.0			15.0	15.0		50.0			50.0	
Actuated g/C Ratio		0.20			0.20	0.20		0.67			0.07	
V/C Ratio		0.47			0.47	0.34		0.53			0.95	
Control Delay		26.2			33.3	7.8		8.7			34.1	
Queue Delay		0.0			0.0	0.0		0.0			0.0	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Total Delay		26.2			33.3	7.8		8.7			34.1	
LOS		С			С	А		А			С	
Approach Delay		26.2			19.8			8.7			34.1	
Approach LOS		С			В			А			С	
Queue Length 50th (ft)		52			51	0		96			303	
Queue Length 95th (ft)		107			101	43		166			#608	
Internal Link Dist (ft)		920			920			920			520	
Turn Bay Length (ft)						30						
Base Capacity (vph)		337			261	404		930			890	
Starvation Cap Reductn		0			0	0		0			0	
Spillback Cap Reductn		0			0	0		0			0	
Storage Cap Reductn		0			0	0		0			0	
Reduced v/c Ratio		0.47			0.47	0.34		0.53			0.95	
Intersection Summary												
Area Type:	Other											
Cycle Length: 75												
Actuated Cycle Length: 7	5											

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 80 Control Type: Pretimed

Maximum v/c Ratio: 0.95

Intersection Signal Delay: 24.2

Intersection Capacity Utilization 90.7%

Intersection LOS: C ICU Level of Service E

Analysis Period (min) 15# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

ø2 (R)	- - 04
55 s	20 s
Ø6 (R)	∲ ∲ ø8
55 s	20 s

0.2

Intersection

Int Delay, s/veh

Movement	EBL	EBT	EBR		WBL	WBT	WBR		NBL	NBT	NBR	SBL	SBT	SBR
Vol, veh/h	0	0	4		5	0	4		1	529	1	2	568	2
Conflicting Peds, #/hr	0	0	0		0	0	0		0	0	0	0	0	0
Sign Control	Stop	Stop	Stop		Stop	Stop	Stop		Free	Free	Free	Free	Free	Free
RT Channelized		-	None		-	-	None		-	-	None	-	-	None
Storage Length	-	-	-		-	-	-		-	-	-	-	-	-
Veh in Median Storage, #	-	0	-		-	0	-		-	0	-	-	0	-
Grade, %	-	0	-		-	0	-		-	0	-	-	0	-
Peak Hour Factor	98	98	98		98	98	98		98	98	98	98	98	98
Heavy Vehicles, %	0	0	4		0	0	0		0	6	0	0	5	0
Mvmt Flow	0	0	4		5	0	4		1	540	1	2	580	2
Major/Minor	Minor2			N	linor1			٨	Naior1			Maior2		
Conflicting Flow All	1120	1128	591		1120	1128	540		582	0	0	541	0	
Store 1	1129 595	595	001		5/2	5/2	540		502	U	0		0	0
Stage 2	500	542	-		597	596	-		-	-	_	_		_
Critical Udway	7 4	040	- 6 24		7 1	500	62		41	-		41	_	_
Critical Houry Sta 1	6.1	0.0	0.24		6.1	0.5	0.2		4.1	-	-	·····		
Critical Howy Sty 1	0.1	0.0	-		0.1	0.0 E E	-		-	-	-	-	-	-
Chlical Huwy Sig Z	0.1	0.0	2 226		2.5	0.0	22		- 22	•	-	- 22		-
Politicar 1 Managura	0.0 400	200	5.550		102	206	5.5		1002	-	-	1029	-	-
Pot Cap-1 Maneuver	100	200	010		100	200	040		1002	-	-	1030	-	-
Stage I	501	501	-		020	523	-		-	-	-	-	-	-
	527	523	-		499	500	-		-	-	-	-	-	-
Platoon blocked, %	404	005	540		404	005	E 4 0		1000	-	-	1020	-	-
Mov Cap-1 Maneuver	181	205	010		101	200	540		1002	-	-	1030	-	-
wov Cap-2 Maneuver	181	205	-		101	200	-		-	•	-	-	-	-
Stage 1	500	499	-		527	522	-		-	-	-	-	-	-
Stage 2	523	522	-		494	499	-		-	-	-	-	-	-
Approach	EB				WB				NB			SB		
HCM Control Delay, s	12.1				19.5				0			0		
HCM LOS	В				С									
Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1W	VBLn1	SBL	SBT	SBR						
Capacity (veh/h)	1002	-	-	510	258	1038	-							
HCM Lane V/C Ratio	0.001	-	-	0.008	0.036	0.002	-	-						
HCM Control Delay (s)	8.6	0	-	12.1	19.5	8.5	0	-						
HCM Lane LOS	0.0 A	Ă	-	В	C	A	Ă	-						
HCM 95th %tile Q(veh)	0	-	-	Ō	0.1	0	-	-						

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			ب ا	۴		\$			\$	
Volume (vph)	42	69	112	78	59	123	35	462	43	188	404	29
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width (ft)	15	15	15	12	12	11	12	12	12	12	12	12
Storage Length (ft)	0		0	0		30	0		0	0		0
Storage Lanes	0		0	0		1	0		0	0		0
Taper Length (ft)	25			25			25			25		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.932				0.850		0.989			0.994	
Flt Protected		0.991			0.972			0.997			0.985	
Satd. Flow (prot)	0	1857	0	0	1754	1531	0	1828	0	0	1836	0
FIt Permitted		0.910			0.575			0.941			0.711	
Satd. Flow (perm)	0	1705	0	0	1038	1531	0	1725	0	0	1326	0
Right Turn on Red			Yes			Yes			Yes			Yes
Satd. Flow (RTOR)		61				119		13			7	
Link Speed (mph)		30			30			30			30	
Link Distance (ft)		1000			1000			1000			600	
Travel Time (s)		22.7			22.7			22.7			13.6	
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Heavy Vehicles (%)	0%	3%	6%	1%	11%	2%	10%	2%	2%	2%	1%	1%
Adj. Flow (vph)	44	72	117	81	61	128	36	481	45	196	421	30
Shared Lane Traffic (%)	_		_	_			_		-	-		
Lane Group Flow (vph)	0	233	0	0	142	128	0	562	0	0	647	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)		0			0			0			0	
Link Offset(ff)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
I wo way Left I urn Lane				4.00	4 00		4.00	4 00	4.00	4 00	4.00	4 00
Headway Factor	0.88	0.88	0.88	1.00	1.00	1.04	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		y	15	6 T A	9	15		9	15 De	N 1.0	9
Turn Lype	Perm	NA		Perm	NA	Perm	Perm	NA		Perm	NA	
Protected Phases		4		•	8	0	0	Z		c	Ö	
Permitted Phases	4	00.0		8	00.0	8	Z	55 A		55.0	55.0	
Minimum Split (s)	20.0	20.0		20.0	20.0	20.0	55.U	55.U		55.U	55.0	
Total Split (S)	20.0	20.0		20.0	20.0	20.0	05.0	0.00		0.00	0.00	
Total Split (%)	20.7%	20.7%		20.7%	20.7%	20.1%	13.3%	13.3%		13.3%	13.3%	
Valley Time (a)	10.0	15.0		10.0	15.0	15.0	0.00	50.0		30.0	30.0	
Tellow Time (S)	4.0	4.0		4.0	4.0	4.0	4.0	4.0		4.0	4.0	
All-Red Time (S)	1.0	1.0		1.0	1.0	1.0	1.0	1.0		1.0	1.0	
Lost Time Aujust (s)		0.0			0.0	0.0 5.0		5.0			0.0 5.0	
		5.0			5.0	5.0		5.0			5.0	
Lead Lag Optimize?												
Act Effet Groop (c)		15.0			15.0	15.0		50.0			50.0	
Actuated a/C Patio		10.0 0.20			0.0 0 20	0.0 0.20		00.0 0.67			00.0 0.67	
No Ratio		0.20			0.20	0.20		0.07 0.40			0.07	
Control Delay		0.00 27 2			17 2	0.02 Q Q		7.8			14.2	
Queue Delay		0.0			0.0	0.0		0.0			0.0	

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Total Delay		27.2			47.3	8.8		7.8			14.2	
LOS		С			D	А		А			В	
Approach Delay		27.2			29.0			7.8			14.2	
Approach LOS		С			С			А			В	
Queue Length 50th (ft)		72			62	3		107			165	
Queue Length 95th (ft)		142			#144	45		171			303	
Internal Link Dist (ft)		920			920			920			520	
Turn Bay Length (ft)						30						
Base Capacity (vph)		389			207	401		1154			886	
Starvation Cap Reductn		0			0	0		0			0	
Spillback Cap Reductn		0			0	0		0			0	
Storage Cap Reductn		0			0	0		0			0	
Reduced v/c Ratio		0.60			0.69	0.32		0.49			0.73	
Intersection Summary												
Area Type:	Other											
Cycle Length: 75												
Actuated Cycle Length: 75	5											
Offset: 0 (0%), Reference	d to phase 2:I	NBTL and	6:SBTL,	Start of (Green							
Natural Cycle: 75												
Control Type: Pretimed												

Maximum v/c Ratio: 0.73

Intersection Signal Delay: 16.2 Intersection Capacity Utilization 115.3% Analysis Period (min) 15 Intersection LOS: B ICU Level of Service H

95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

ø2 (R)	ø4
55 s	20 s
Ø6 (R)	₩ Ø8
555 s	20 s

0.3

Intersection

Int Delay, s/veh

Vol, veh/h 2 0 3 3 0 3 4 654 5 5 591 0 Conflicting Peds, #/hr 0
Conflicting Peds, #/hr 0
Sign Control Stop Stop
RT Channelized - - None
Storage Length - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 0 0 0 0 0 0 0 0 0 0 0 1 4 4 - - - - - - - - - - - -
Veh in Median Storage, # - 0 - 0 - 0 - 0 - 0 - 0 - 0 0 0 0 0 0 0 0 1 4 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 </td
Grade, % - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - Peak Hour Factor 98
Peak Hour Factor 98
Heavy Vehicles, % 0 0 0 0 0 0 0 0 2 0 1 4 Mvmt Flow 2 0 3 3 0 3 4 667 5 5 603 0 Major/Minor Minor2 Minor2 Minor1 Major1 Major2 Conflicting Flow All 1293 1294 603 1293 1291 670 603 0 672 0 0 Stage 1 613 613 - 678 678 -
Mvmt Flow 2 0 3 3 0 3 4 667 5 5 603 0 Major/Minor Minor2 Minor1 Major1 Major2 Conflicting Flow All 1293 1294 603 1293 1291 670 603 0 672 0 0 Stage 1 613 613 - 678 678 -
Major/Minor Minor2 Minor1 Major1 Major2 Conflicting Flow All 1293 1294 603 1293 1291 670 603 0 672 0 0 Stage 1 613 613 - 678 678 -<
Conflicting Flow All 1293 1294 603 1293 1291 670 603 0 672 0 0 Stage 1 613 613 - 678 678 -
Stage 1 613 613 - 678 678 -
Stage 2 680 681 - 615 613 -
Critical Hdwy 7.1 6.5 6.2 7.1 6.5 6.2 4.1 - 4.1 - Critical Hdwy Stg 1 6.1 5.5 - 6.1 5.5 -
Critical Hdwy Stg 1 6.1 5.5 - 6.1 5.5 -
Critical Hdwy Stg 2 6.1 5.5 -
FONOW-ND FIGWY 35 4 33 35 4 33 77 77
Pot Cap-1 Maneuver 141 164 503 141 165 460 984 928
Stage 1 483 486 - 445 455
Stage 2 444 453 - 482 486
Platoon blocked %
Mov Cap-1 Maneuver 139 162 503 139 163 460 984 928
Mov Cap-2 Maneuver 139 162 - 139 163
Stage 1 480 482 - 442 452
Stage 2 438 450 - 475 482 -
Approach EB WB NB SB
HCM Control Delay S 19.9 22.4 0.1 0.1
HCM LOS C C
Minor Lane/Major Mymt NBL NBT NBR FBL n1WBL n1 SBL SBT SBR
$Canacity (veh/b) \qquad 0.84 \qquad - \qquad 246 213 0.28 \qquad - \qquad $
HCM Lane V/C Ratio $0.004 0.021 0.029 0.005$
HCM Control Delay (s) $87 0 - 199 224 89 0 -$
HCM control Doily (5) $0.7 = 10.0 \times 22.4 = 0.0 = 0.0 \times 10^{-1}$
HCM 95th %tile Q(veb) 0 01 01 0

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